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## Highlights

### **Energetics of tidally induced internal waves over isolated seamount**

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- The study focuses on the tidal energy conversion to internal waves over an isolated seamount.
- Sensitivity runs were conducted in a wide range of the numerical grid resolution.
- The coarse grid models overestimate available potential energy converted to internal waves.

# Energetics of tidally induced internal waves over isolated seamount

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## Abstract

Tidally generated internal waves over Rosemary Bank Seamount, North Atlantic, were investigated using the Massachusetts Institute of Technology general circulation model. The model results were validated against in-situ data collected during the 136th cruise of the RRS ‘James Cook’ in June 2016. The current study focuses on the sensitivity of the model output to the parameter settings. The estimates of the available potential energy integrated over the model domain were taken as a proxy for evaluating the sensitivity of the model results to the grid steps, horizontal and vertical viscosity, diffusivity, and mixing schemes. It was found that coarse grid models overestimate available potential energy converted to internal tides over seamounts. In fact, the energy conversion rate from barotropic to baroclinic tidal components is sensitive to the grid resolution. The reasons for this tendency are discussed in the paper.

*Keywords:*

Internal tide, Rosemary Bank Seamount, Numerical modelling

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## 1. Introduction

2 The principal sources of the tidal energy conversion from barotropic to  
3 baroclinic motions are located over oceanic ridges, continental slopes and  
4 seamounts. These areas provide a basic income to the baroclinic wave en-  
5 ergy, which ultimately converts into internal water mixing and provides the  
6 conditions for setting the global oceanic circulation (Munk and Wunsch, 1998).

7 Analysis of the parameterization of internal wave effects for setting the  
8 global oceanic stratification was recently estimated by MacKinnon et al.

9 (2017). The authors discussed tidally induced mixing over bottom obsta-  
10 cles and estimated how much tidal energy is radiated to the far-field with  
11 internal waves. The lee wave mechanism of internal wave generation was the  
12 focus of this study. This scenario takes place under supercritical tidal  
13 conditions when the tidal flow is strong enough to arrest the generated internal  
14 waves in the area of topographic features. The modelling results presented  
15 by MacKinnon et al. (2017) assume that further steps in the parameteriza-  
16 tion of water mixing are required for making the model predictions accurate.  
17 A very detailed analysis of the tidal energy conversion and contribution of  
18 higher baroclinic modes to the energy balance was conducted recently by Vic  
19 et al. (2019). Using a semi-analytical model, the authors found that higher  
20 baroclinic tidal modes can account for up to 27% of tidal energy conversion.

21 Note that coarse-grid ocean models cannot resolve internal lee waves and  
22 short-scale internal modes. As a consequence, these processes are missing in  
23 model energy estimates. However, the comparison of fine and coarse resolu-  
24 tion model outputs can evaluate the effect of the sub-grid baroclinic process  
25 on the energy budget. The model settings can be the same except for the  
26 grid resolution in both cases. Such experiments help understand the role of  
27 small-scale processes in water mixing and energy budget.

28 The present paper focuses on Rosemary Bank Seamount (RBS) located  
29 in the North Atlantic, Figure 1. This case study aims to understand the  
30 sensitivity of model predictions to the model settings. 136th cruise of the  
31 RV "James Cook" was conducted in the RBS area in May-June 2016 (here-  
32 after JC136). The data collected during this cruise are considered in the  
33 present paper. Specifically, we refer to the temperature, salinity, temperature  
34 and velocity profiles recorded at three CTD-LADCP stations (Connectivity-  
35 Temperature-Depth, Lowered-Acoustic-Doppler-Current-Profiler). The po-  
36 sitions of oceanographic stations are shown in Figure 1 a.

37 Theoretical analysis of the tidally induced internal waves around RBS  
38 was reported in (Stashchuk and Vlasenko, 2021). It was found there that  
39 internal wave dynamics, specifically, the wave generation and their propa-  
40 gation over RBS, can be treated in terms of two waveguides located in the  
41 seasonal and main pycnoclines, Figure 1 a. Specifically, the tidal flow in-  
42 teracting with a cluster of volcanic origin tall bottom cones located at the  
43 RBS summit (see Figure 1 a) generates short-scale internal waves in subsur-  
44 face 100 m thick seasonal pycnocline layer. Below 800m depth, i.e. in the  
45 main pycnocline, Figure 1 b, oscillating tidal flow generates bottom trapped  
46 sub-inertial internal waves propagated counterclockwise around RBS.

47 The numerical experiments reported in (Stashchuk and Vlasenko, 2021)  
48 revealed a good agreement between the model and observational data. The  
49 present study is based on the concept of two waveguides reported in the  
50 paper mentioned above. The intensification of the baroclinic tidal signal in  
51 the surface and bottom layers is evident both in observations (Figure 2 a,b)  
52 and the model outputs (Figure 2 c,d).

53 The present study focuses on the requirements that should be applied  
54 to large-scale modelling. In many global ocean models, the horizontal grid  
55 resolution is relatively coarse, several kilometres in the best-case scenario.  
56 The model requirements for simulations of tidally induced baroclinic motions  
57 are more demanding. In many cases, the horizontal grid resolution should be  
58 100 m or less for accurate replication of generated internal waves. The global  
59 oceanic models are incapable of simulating internal tides with such grids on  
60 global and regional scales (Robertson, 2006). We consider the RBS area as  
61 a case study in the context of broader applications of the modelling efforts.

62 Structure wise, the paper is arranged as follows. It starts with the model  
63 description. This section is followed by a discussion of the baroclinic tidal  
64 energy estimation method. The grid resolution and the turbulent mixing  
65 parameterizations are discussed in the section "Model results". Finally, the  
66 principal outcomes of the study are formulated in the concluding section.

## 67 **2. The model**

68 The modelling experiments were conducted using the fully non-linear non-  
69 hydrostatic Massachusetts Institute of Technology general circulation model  
70 (MITgcm) (Marshall et al., 1997). The model domain, Figure 1 a, included a  
71  $815 \times 698$  numerical grid with horizontal resolution 115 m in its central part.  
72 A telescopic increase of the spatial resolution was arranged by adding extra  
73 128 grid points to the lateral boundaries of the calculation area. In doing  
74 so, a smooth increase of the horizontal resolution from 115 m in the central  
75 part to  $2 \cdot 10^8$  m at the periphery allowed to avoid the wave reflection from  
76 the model boundaries. The water depth was restricted by 2000 m isobath in  
77 the vertical direction. The vertical grid step was ten metres in all numerical  
78 experiments.

79 The shaved cell method for the topography interpolation was used in the  
80 present study. Its advantage, compared to the traditional full step repre-  
81 sentation, is in the reduction of numerical errors induced by the incorrect  
82 bathymetry interpolation. This problem was discussed by Adcroft et al.

83 (1997). It was demonstrated there that the shaved cell method for the to-  
 84 pography interpolation shows a substantial improvement in the consistency  
 85 of the model results with the observational data compared with the tradi-  
 86 tional full step topography representation. The partial cell capability can be  
 87 used with the variable parameter called in the MITgcm as *hFacMin* (value  
 88 between 0 and 1). It corresponds to the minimum fractional size of the cell.  
 89 In the present calculation, we have been using *hFacMin*=0.2.

90 The tide forcing was activated in the model by a tidal potential added  
 91 to the right-hand side of the momentum balance equations. The details of  
 92 the method are described in (Vlasenko and Stashchuk, 2021). Considering  
 93 that M<sub>2</sub> tidal signal predominates in the RBS area, we restricted our analysis  
 94 using only principal semidiurnal tidal forcing. The tidal input parameters  
 95 were set using the data taken from the inverse tidal model TPXO 8.0 (Egbert  
 96 and Erofeeva, 2002). The model was run with a steady, uniform horizontal  
 97 stratification assuming no initial horizontal pressure gradients.

98 The Richardson number dependent parametrization, PP81, was used for  
 99 the coefficients of vertical viscosity  $A^h$  and diffusivity  $K^h$  (Pacanowski and  
 100 Philander, 1981). The details are as follows:

$$\begin{aligned} A^v &= \frac{A_0^v}{(1+a\text{Ri})^n} + A_b^v, \\ K^v &= \frac{A^v}{(1+a\text{Ri})} + K_b^v. \end{aligned} \quad (1)$$

101 Here  $Ri$  is the Richardson number,  $Ri = N^2(z)/(u_z^2 + v_z^2)$ , and  $u$  and  $v$  are  
 102 the components of zonal and meridional horizontal velocities, respectively.  
 103 The background mixing/viscosity model parameters  $A_b$  and  $K_b$  were set at  
 104 the minimum level to provide the conditions for internal waves generation  
 105 and propagation:  $A_b^v=10^{-5} \text{ m}^2 \text{ s}^{-1}$  and  $K_b^v=10^{-5} \text{ m}^2 \text{ s}^{-1}$ . The adjustable  
 106 parameters were:  $A_0^v=1.5 \cdot 10^{-2} \text{ m}^2 \text{ s}^{-1}$ ,  $a=5$  and  $n=1$ . This set of model  
 107 parameters revealed the excellent performance of the MITgcm in replication  
 108 of tidally generated internal waves (Stashchuk et al., 2014; Stashchuk and  
 109 Vlasenko, 2017; Vlasenko et al., 2014, 2018).

110 The PP81 parameterization increases the coefficients  $A^v$  and  $K^v$  in the  
 111 areas with small Richardson numbers, which dumps shear instabilities and  
 112 smooths inverse water stratification produced by breaking internal waves. It  
 113 also allows setting the upper limit of the vertical viscosity coefficient  $A_{\text{max}}^v$ .  
 114 In this study  $A_{\text{max}}^v$  was taken at the level of  $0.1 \text{ m}^2 \text{ s}^{-1}$ .

115 The vast majority of the model runs in this study were conducted for the  
 116 time interval of six days (144 hours) with the constant horizontal viscosity

117  $A^h$  and diffusivity  $K^h$  coefficients equals  $0.5 \text{ m}^2 \text{ s}^{-1}$ . Additional sensitivity  
118 runs were done in a wide range of diffusivity/viscosity parameters. They are  
119 discussed below.

120 Computing wise, one-hour outputs were arranged for all three-dimensional  
121 fields. In addition, vertical profiles of temperature and horizontal velocities  
122 were recorded with one-minute sampling at some selected points. Their po-  
123 sitions coincide with the CTD-LADCP stations.

### 124 **3. Tidal energy estimation method**

125 The tidal energy conversion rate from barotropic to baroclinic component  
126 depends on many factors. They are the intensity of the tidal flow, water  
127 stratification, the shape of bottom topography, background mixing processes,  
128 etc. The sink of tidal energy to internal waves and ultimately to water mixing  
129 can be quantified in terms of internal tidal energy generated over the bottom  
130 topography.

131 In many cases, it is not easy to separate the barotropic tidal signal from  
132 the baroclinic one. Specifically, this is true when velocities are recorded  
133 over an inclined three-dimensional bottom topography. In this case, the  
134 separation procedure can introduce a significant error.

135 The residual currents generated by tides can lead to extra uncertainty in  
136 the calculations of a vertical mean tidal velocity. Specifically, this concerns  
137 the case of bottom trapped waves. Such a case was reported by Lerczak et  
138 al. (2003) who studied internal wave dynamics at the Mission Beach (USA).  
139 Analysing the ADCP data, they found differences in the structure of along-  
140 shore and cross-shore tidal currents. The authors pointed out that separating  
141 the barotropic tidal signal from the baroclinic one should be used with cau-  
142 tion, particularly in regions with significant topographic variations. Note  
143 that the estimates of available potential energy produced by tides are less  
144 sensitive to the barotropic component. The analysis presented below is based  
145 on the estimation of the APE.

146 Several methods are used for the APE calculations. A comprehensive  
147 analysis of the procedures applied to internal wave fields was presented by  
148 Kang and Fringer (2010). Three commonly used methods for the APE esti-  
149 mates suggested by Lorenz (1955), Gill (1982), and Holliday and McIntyre  
150 (1981) are considered in this paper. It was found that the method reported  
151 by Holliday and McIntyre (1981) is the most accurate in the calculation of  
152 the APE for internal waves. Their technique is based on the Taylor series

153 analysis. The recommended formula for the APE estimates is as follows:

$$\text{APE} = \frac{g^2 \rho'^2}{2\rho_0 N^2} + \frac{g^3 (N^2)_z \rho'^3}{6\rho_0^2 N^6} + O(\rho'^4). \quad (2)$$

154 Here  $\rho'$  is the perturbation of density to its equilibrium state.

155 Algorithm (2) was used in this paper. The APE calculations were con-  
156 ducted every one hour using the model outputs. The graphs are presented  
157 below in the following sections. Technically, the APE was calculated by verti-  
158 cal and horizontal integration over the whole model domain. The quadratic  
159 polynomial fit that includes the three nearest grid points best fits for the  
160 volume integrated APE and presents the long-term trend

#### 161 4. Model results

162 The sensitivity of the model output to the horizontal and vertical grid  
163 resolution is reported in this section. The principal point of this study is:  
164 what the horizontal and vertical grid steps  $\Delta x$  and  $\Delta z$  should be taken to  
165 resolve the baroclinic tidal processes correctly? Vitousek and Fringer (2011)  
166 have shown that the ability of the model to reproduce small-scale nonhydro-  
167 static physical processes depends on the leptic ratio coefficient,  $\lambda \equiv \Delta x/h_1$ .  
168 Here  $h_1$  is the depth of the interface/pycnocline. For an accurate replication  
169 of the internal wave dynamics produced by non-hydrostatic models, the value  
170 of the leptic ratio  $\lambda$  should be at the level of  $O(1)$  (Vitousek and Fringer,  
171 2011).

172 Considering these requirements, one should mention that the water strat-  
173 ification in the RBS area has two principal elements shown in Figure 1 b: a  
174 shallow 100-metre depth seasonal pycnocline and the main pycnocline lo-  
175 cated below 1000 m depth. The latter is weaker but occupies a much larger  
176 part of the water column.

177 Numerically wise, both values of  $h_1$  for seasonal and main pycnoclines can  
178 be taken to estimate the leptic ratio. These estimates can help in the choice  
179 of the model resolution. The principal question is: what processes should  
180 be replicated by the model? The fine resolution modelling allows consider-  
181 ing a wide variety of small-scale dynamics, both short-scale internal waves  
182 developed in seasonal pycnocline and bottom trapped internal tidal waves.  
183 These requirements are not always possible for global-scale models. We con-  
184 sider a range of grid settings to illustrate models' abilities to replicate the  
185 wide-scale baroclinic tidal motions. The study discusses fine-scale resolution



186 model experiments and analyses the coarser grid runs used in global ocean  
187 models.

#### 188 *4.1. Sensitivity to the grid resolution*

189 An example of the model sensitivity to the grid resolution is shown in  
190 Figure 3. The model temperature time-series at station 32 (Figure 1 a) was  
191 calculated with different horizontal grid steps, 111.75 m, 463 m, and 926 m.  
192 They are presented in panels a, b, and c of Figure 3, respectively. This figure  
193 reveals that the ability of the model to capture short internal waves in the  
194 upper seasonal pycnocline layer decreases with the increase of horizontal grid  
195 steps. However, the numerical scheme still works well with coarser resolution  
196 and reproduces long wave oscillations. Note that long-term wave amplitudes  
197 increase with the increase of the horizontal grid steps.

198 How sensitive are the tidally induced baroclinic motions and water mixing  
199 to the model resolution? The coarser grid model predictions of internal tidal  
200 energy could differ from that estimated in the fine-resolution experiments.  
201 The influence of the horizontal step on the value of APE is illustrated in  
202 Figure 4 a. Here a six-day time series of the depth-integrated model domain  
203 APE calculated for the horizontal resolution  $\Delta x = \Delta y = 111.75$  m, 463 m, and  
204 926 m are presented. The parameters  $A^h = K^h$  in these experiments were  
205  $0.5 \text{ m}^2 \text{ s}^{-1}$ , and the vertical resolution  $\Delta z$  was equal to 10 m.

206 The common feature of all three graphs is the evidence of tidal periodicity.  
207 The fit curves to these periodical oscillations show the steady growth of the  
208 APE. However, after six days of tidal motion, the system ultimately arrives  
209 at a stationary state.

210 The coarser grids usually dump short internal waves, which reduces the  
211 APE in the numerical predictions. At the same time, coarser grids do not  
212 affect the generation of long internal waves, which are more energetic than  
213 short-scale waves. To have some quantitative estimates, a series of numeri-  
214 cal experiments with different grid resolutions, horizontal and vertical, was  
215 conducted to study the sensitivity of the model outputs to the model grid  
216 parameters.

217 The APE time series for a wide range of model resolution with horizontal  
218 grid steps from 115 m to 926 m, and vertical grid steps from 5 m to 20 m are  
219 presented in Figures 4 a and 4 b. These figures show the spin-up of the model  
220 over about 150 hours. The model comes to a stationary regime at the end  
221 of this time interval, although the domain integrated APE is sensitive to the  
222 model resolution. It is generally higher at coarser grids.

223 There are several explanations for this result. The first one can be found  
224 considering the domain volume. The latter is sensitive to the grid resolution.  
225 It varies with changing vertical and horizontal model grid steps, Figure 4 c  
226 and 4 d. The MITgcm is a  $Z$ -coordinate model which approximates the  
227 bottom as a step-wise function. The bottom topography in  $Z$ -coordinate  
228 models and the total water volume varies depending on the grid resolution.  
229 For instance, the total volume of water in the model domain for the coarser  
230 experiment shown in Figure 4 exceeds the fine-resolution volume for more  
231 than 2%. In addition, the topography in the coarser grid is steeper. The  
232 increase of the bottom steepness results in the generation of more energetic  
233 bottom-trapped internal waves, Figure 3.

234 The confirmation of the APE growth due to roughening of topography is  
235 seen in Figure 4 b. It shows the domain-integrated APE time series for three  
236 different vertical grid steps, 5 m, 10 m, and 20 m. Quantitatively, decreasing  
237 the vertical resolution in  $Z$ -coordinate models increases the water volume in  
238 the regions of sloping topography. As a result, the total APE calculated at  
239 coarser grids is higher, Figure 4 d. Making the vertical resolution thinner  
240 leads to improvements in the replication of the bottom flow dynamics.

241 Considering some local characteristics (not the domain integrated), the  
242 sensitivity of the model output to the grid resolution can be more detailed.  
243 Two examples of this sensitivity are shown in Figure 5. The model predicted  
244 temperature calculated at the positions of CTD stations 31 and 33 shows the  
245 consistency of all time-series considered with different horizontal and verti-  
246 cal grid resolutions. The tidal nature of vertical oscillations is clearly seen in  
247 these records. All curves reveal in-phase tidal periodicity. The amplitudes of  
248 vertical oscillations for all model outputs are also comparable. That could  
249 be evidence that coarse grid models can capture the main energy contributor  
250 with acceptable accuracy. At the same time, decreasing horizontal and verti-  
251 cal model resolution introduces some more details that can be very important  
252 for predicting local marine environment parameters.

#### 253 *4.2. Sensitivity to horizontal mixing parameterization*

254 The time series of the model predicted APE calculated for different model  
255 settings, e.g. diffusivity, viscosity and grid resolution, are compared in this  
256 section. By making the grid finer, at some stage the model output starts to  
257 be insensitive to further reduction of the grid step.

258 Figures 6 shows the domain integrated APE and its best fit for different  
259 values of the viscosity coefficients: 0, 0.01, 0.5, 50 m<sup>2</sup>s<sup>-1</sup>. All curves presented

260 here show that the tidal energy increases gradually after the model starts.  
 261 The spin-up period, 150 hours, is shown in Figure 6. The system becomes  
 262 stationary when the pumping tidal energy is balanced by dissipation. As  
 263 we found, the model predicted volume integrated APE capacity in the area  
 264 does depend on the horizontal mixing parameterization. For the horizontal  
 265 mixing/viscosity coefficients between  $0.01 \text{ m}^2 \text{ s}^{-1}$  and  $50 \text{ m}^2 \text{ s}^{-1}$  the APE level  
 266 varies in the range of 100 %, Figure 6. This fact should be taken into account  
 267 in the interpretation of large-scale circulation modelling results.

### 268 *4.3. Experiments with vertical mixing schemes*

269 In large-scale models, the energy cascading along the spectrum is gen-  
 270 erally provided, introducing parameterization schemes for vertical viscosity  
 271 and diffusivity. One of them is the Richardson number based parameteriza-  
 272 tion (1) included in the MITgcm package as a standard option. It shows a  
 273 good performance for internal tide modelling in many studies, e.g. Vlasenko  
 274 et al. (2014, 2016, 2018); Vlasenko and Stashchuk (2018).

275 Field measurements (Polzin et al., 1997) have revealed that vertical mix-  
 276 ing does not occur uniformly over the oceans. It is normally enhanced near  
 277 rough topographies due to the generation of internal waves that convert  
 278 to turbulence. The lower level background mixing develops at the level of  
 279  $\sim 10^{-5} \text{ m}^2 \text{ s}^{-1}$  over the whole ocean interior (Ledwell et al., 1998; Gregg, 1989).  
 280 This value can be three orders of magnitude larger **over rough topography**  
 281 **features**, (Polzin et al., 1997). To have a comparison, the results presented  
 282 below show the model outputs calculated for two MITgcm build-in vertical  
 283 mixing schemes. In all experiments, the horizontal grid resolution was 463 m.

#### 284 *4.3.1. Richardson number dependent scheme PP81*

285 The Richardson number dependent parameterization for vertical mixing  
 286 (1) was used in this study. The value  $0.1 \text{ m}^2 \text{ s}^{-1}$  of the maximum permis-  
 287 sible viscosity coefficient  $A_{\text{max}}^v$  was taken in this study. This requirement  
 288 is applied in the MITgcm setting for the areas with strong vertical mixing,  
 289 assuming possible density inversions. Note that the background turbulent  
 290 mixing was set at the level of  $A_b^v = 10^{-5} \text{ m}^2 \text{ s}^{-1}$  and  $K_b^v = 10^{-5} \text{ m}^2 \text{ s}^{-1}$  in the  
 291 whole area.

292 The sensitivity of the model outputs to the viscosity coefficient  $A_{\text{max}}^v$  was  
 293 checked by changing this parameter within a two-order range. The result is  
 294 shown in Figure 7. It illustrates that the increase of  $A_{\text{max}}^v$  from 0.001 to  
 295  $0.1 \text{ m}^2 \text{ s}^{-1}$  leads to stabilizing of the model output. Comparing the time

296 series of temperature records calculated for Station 32 with different  $A_{\max}^v$   
297 coefficients, Figures 7 a and 7 b, indicates that the choice  $A_{\max}^v=0.1 \text{ m}^2 \text{ s}^{-1}$   
298 shows a more stable model output.

#### 299 *4.3.2. KL10 mixing scheme*

300 Klymak and Legg (2010) developed an original mixing scheme that is  
301 focused on the effect of breaking internal waves and does not include the  
302 Richardson-number criterion. This scheme assumes that energy dissipa-  
303 tion is governed by the equivalence of the density overturning scales to the  
304 Ozmidov scale. Eddy diffusivity and viscosity are estimated using the Os-  
305 born relation (Osborn, 1980). This method yields a simple parameterization  
306  $Kz = 0.2L_T^2N$ , where  $L_T$  is the size of vertical density overturns. This  
307 method is included in the MITgcm as the KL10 package. It was scrutinized  
308 by Klymak et al. (2013) that this parameterization does not account for  
309 shear-driving mixing.

310 A series of experiments were conducted in the present study with KL10  
311 mixing scheme. An example of typical time series of the APE calculated for  
312 station 32 is shown in Figure 7 c. For the comparison, panels a and b show  
313 similar time series calculated using the PP81 scheme with different maximum  
314 permissible viscosity coefficients  $A^v$ . All other model parameters were the  
315 same in these experiments.

316 Note that at a local scale, a two-order decrease of the maximum vertical  
317 viscosity coefficient results in the appearance of instabilities that are visible in  
318 the time series, Figure 7 b. Comparison of Figures 7 a and 7 b indicates that  
319 the choice  $A_{\max}^v=0.1 \text{ m}^2 \text{ s}^{-1}$  is the more realistic one producing a more stable  
320 vertical structure (without inversions) usually observed in the ocean. The  
321 KL10 parameterization reproduces both long-period internal waves in the  
322 bottom layer and short-period waves in the surface layer quite successfully,  
323 Figure 7 b, although the signal looks less regular than that produced by the  
324 PP81 scheme, Figure 7 a.

325 Figure 8 b shows the APE time series obtained with the PP81 and KL10  
326 schemes. Both APE curves are close to each other over 93 hours of the model  
327 run. However, after eight tidal cycles, the APE calculated using the KL10  
328 scheme continues to grow above the already saturated APE level achieved  
329 by the PP81-scheme.

## 330 5. Discussion and conclusions

331 Tidal energy conversion from barotropic to baroclinic components is one  
332 of the principal driving forces of the global ocean mixing and meridional  
333 overturning circulation (Munk and Wunsch, 1998). This process is still not  
334 well resolved in global ocean models. Specifically, the question is to what  
335 extent the tidal energy conversion is sensitive to the models' settings. Grid  
336 resolution, vertical turbulent mixing parameterization, and horizontal viscos-  
337 ity/diffusion settings are critical for a robust model prediction.

338 In previous studies, the authors achieved a good agreement between the  
339 model outputs and field observations (Stashchuk et al., 2014; Stashchuk and  
340 Vlasenko, 2017; Vlasenko et al., 2014, 2018). In this paper, a similar range of  
341 input model parameters is used. In the RBS area, the comparative analysis  
342 of model results and in situ data collected during JC136 cruise was reported  
343 in (Stashchuk and Vlasenko, 2021). The consistency of the model outputs  
344 with the in-situ collected data was demonstrated. The present paper con-  
345 siders the problem in a broader context, assuming that large-scale numerical  
346 models usually use coarse numerical grids and can not include fine-scale baro-  
347 clinic processes. The present paper estimates the possible effect of numerical  
348 grid resolution and turbulent mixing parameterization schemes on the model  
349 output. The principal aim was to find the range of the model applicability  
350 and its sensitivity to the input parameter settings.

351 It was found that the increase of the grid step leads to a damping of  
352 the generation of short internal waves. This result was entirely expected,  
353 assuming higher numerical viscosity at coarser grids. A surprising outcome  
354 was the increase of the domain integrated APE at coarser numerical grids.  
355 The answer was found in terms of the model topography variations presented  
356 at different grid resolutions.  $Z$ -coordinate numerical models reproduce the  
357 bottom topography steeper at coarser grids, affecting the model performance  
358 and intensifying the generated waves.

359 The estimates of the tidally induced kinetic energy ( $K$ ) accumulated in  
360 the area over one tidal cycle has shown the following results:  $K = 3.814 \cdot 10^{13}$  J  
361 for the grid  $\Delta x = \Delta y = 115.75$  m,  $K = 3.8337 \cdot 10^{13}$  J for the grid  $\Delta x =$   
362  $\Delta y = 463$  m, and  $K = 4.0357 \cdot 10^{13}$  J for the grid  $\Delta x = \Delta y = 926$  m. The  
363 vertical resolution  $dz$  and the background horizontal viscosity  $A_b^v$  were the  
364 same in all these experiments, i.e.  $dz = 10$  m and  $A_b^v = 0.5 m^2 s^{-1}$ , respec-  
365 tively. Thus, it was found that both available potential energy and the kinetic  
366 energy increase in the model outputs on coarser grids.

367 The energy conversion rate from barotropic tidal component to internal  
 368 waves in the RBS area was estimated. The calculations were conducted using  
 369 the methodology suggested by Kelly et al. (2010); Zhang et al. (2017). The  
 370 energy conversion  $EC$  for the domain  $L_x \times L_y$  was calculated as:

$$EC = \int_0^{L_x} \int_0^{L_y} \langle p' \vec{U} \nabla H \rangle dx dy. \quad (3)$$

371 Here  $\langle \cdot \rangle$  means the time-averaging over one tidal cycle,  $\vec{U}$  is the depth-  
 372 averaged horizontal velocity, and  $p'$  is the wave-induced pressure perturbation.  
 373 It was found that  $EC = 3.35 \cdot 10^8$  W for a grid  $\Delta x = \Delta y = 115.75$  m,  
 374  $EC = 3.32 \cdot 10^8$  W for the grid resolution  $\Delta x = \Delta y = 463$  m, and  $EC = 2.97 \cdot 10^8$  W  
 375 for the grid  $\Delta x = \Delta y = 926$  m. The vertical step for all considered experi-  
 376 ments was the same, equals  $\Delta z = 10$  m. Our experiments clearly show that  
 377 the energy conversion rate from surface tides to baroclinic motions is under-  
 378 estimated in coarser grid experiments.

379 A similar analysis of the sensitivity of the energy conversion rate to the  
 380 horizontal grid spacing was conducted by Niwa and Hibiya (2011) (for Global  
 381 Ocean) and Zilberman et al. (2009) (for the Mid-Atlantic Ridge). These au-  
 382 thors used quite a different numerical approach than applied in the present  
 383 paper. Specifically, the terrain-following sigma-coordinate hydrostatic mod-  
 384 els were applied to these calculations. It was found there that the tidal energy  
 385 conversion rate integrated over the global ocean (Niwa and Hibiya, 2011) and  
 386 local area in the Brazil Basin (Zilberman et al., 2009) increases with the re-  
 387 duction of the model grid spacing. This conclusion is in line with the results  
 388 reported here obtained by using the  $z$ -coordinate MITgcm model.

389 A methodological outcome from this study is that simple estimations of  
 390 the available potential energy and the total kinetic energy generated by the  
 391 tides over RBS show the increase of these values on coarser model grids,  
 392 Figure 6 a and b. At the same time, the estimates of the energy conversion  
 393 rate from barotropic to internal tide reveal that the coarser grids reduce the  
 394 efficiency of the tidal energy conversion. There is no contradiction between  
 395 these two tendencies. Analysis of Figure 4 c and 4 d shows that the coarser  
 396 grids incorporate larger volumes of water with the increase of the grid step.  
 397 In fact, with the coarser grids, the topography's tidal activity is different  
 398 from that simulated over the fine-resolution topography.

399 A series of numerical experiments were also conducted to test the model  
 400 output's sensitivity to the choice of diffusivity/viscosity model coefficients.

401 Water mixing parameterization is critical for accurately modelling various  
402 processes, from microscopic to global atmospheric and oceanic scales. In the  
403 present study, we used the Richardson-number dependent parameterization  
404 scheme PP81. This turbulent closure scheme provides the APE saturation  
405 over eight tidal cycles. The Osborn relation based scheme KL10 also re-  
406 vealed a similar performance over 7.5 tidal periods. Note that its further  
407 performance over ten tidal cycles did not demonstrate any tendency to reach  
408 the stationary level. In general, the usage of two vertical turbulent mixing  
409 schemes, PP81 and KL10, did not significantly differ the model output over  
410 several tidal cycles, although the KL10 closure model shows a higher internal  
411 tidal energy saturation level.

## 412 **6. Acknowledgement**

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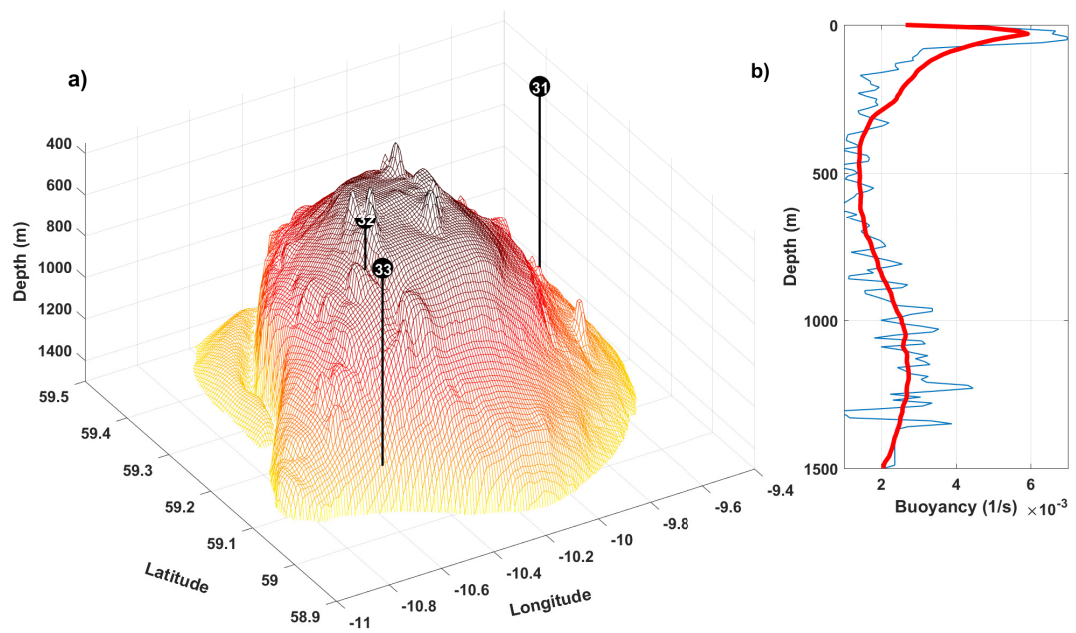


Figure 1: a) Bottom topography of Rosemary Bank Seamount (RBS) with the location of CTD stations 31, 32, and 33 conducted during the 136th cruise of the RV "James Cook". b) The buoyancy frequency recorded in the RBS area is shown in blue. The smoothed buoyancy frequency profile used in the modelling is shown in red.

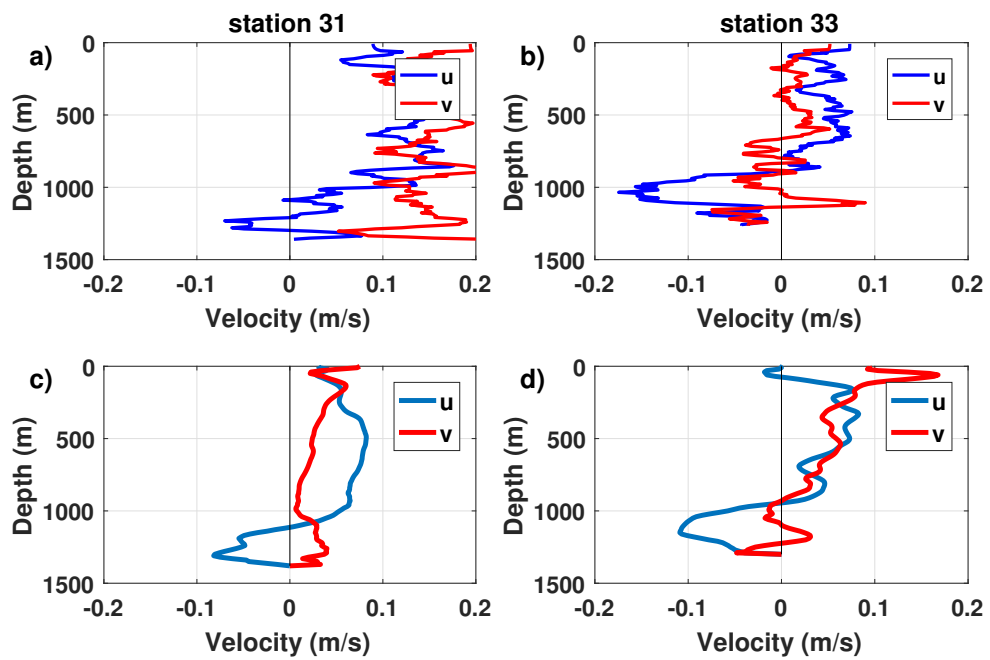


Figure 2: Vertical profiles of zonal (blue) and meridional (red) velocities recorded by the LADCP at 31-st and 33-rd CTD stations (panels a and b, respectively). Panels c and d present the same profiles but replicated by the numerical model.

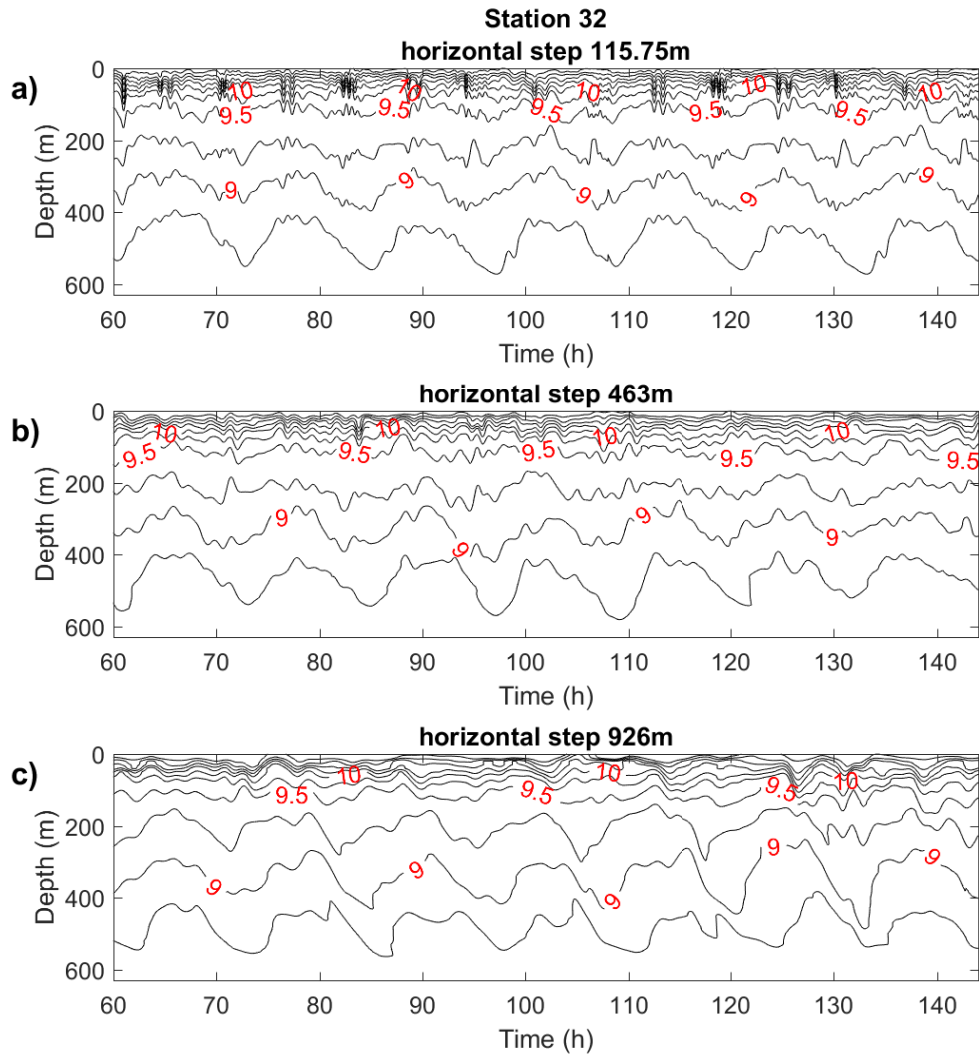


Figure 3: Temperature time series reproduced by the MITgcm at the 32-nd CTD station (the position is shown in Figure 1). The horizontal grid step in these experiments was 115.75 m, 463 m, and 926 m (panels a, b, c, respectively).

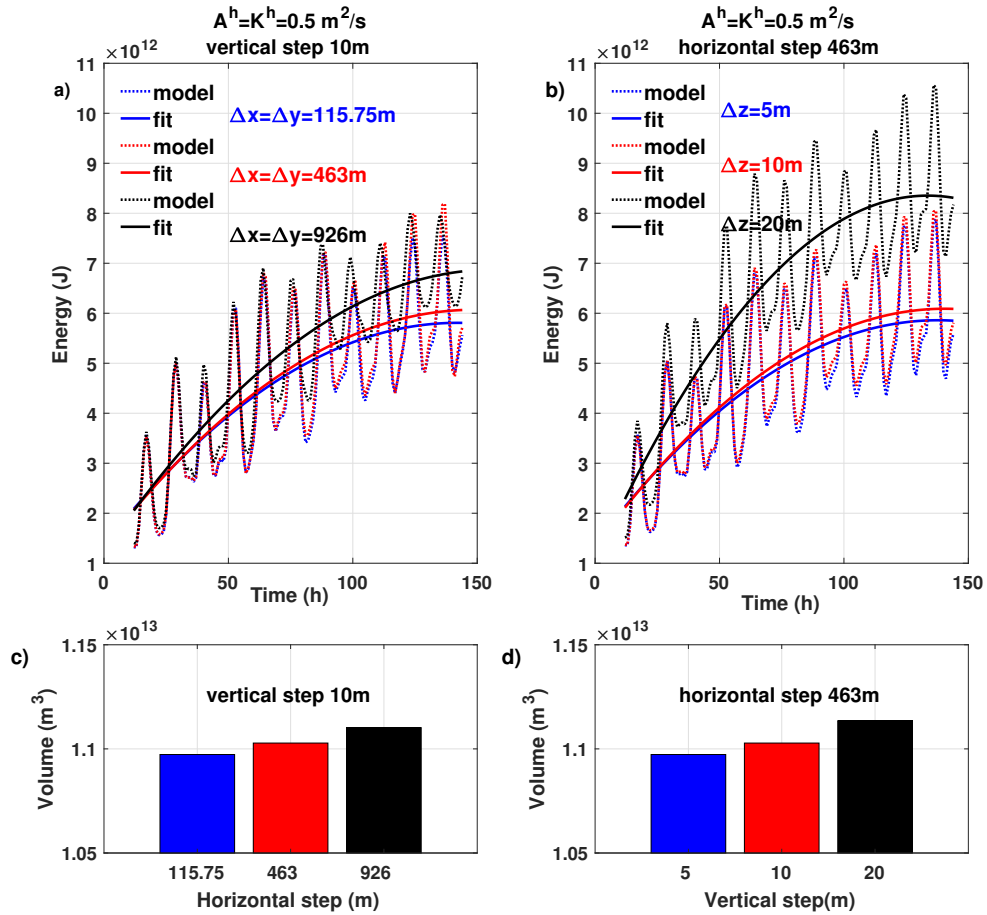


Figure 4: a) Model predicted available potential energy (APE) calculated for the RBS area with a different vertical grid resolution: 115.75m (blue), 463m (red) and 926m (black). b) The same, but calculated with different vertical steps: 5m (blue), 10m (red) and 20m (black). c) and d) The volume of the model domain calculated for different horizontal and vertical grid resolutions. The values are shown in the graph.

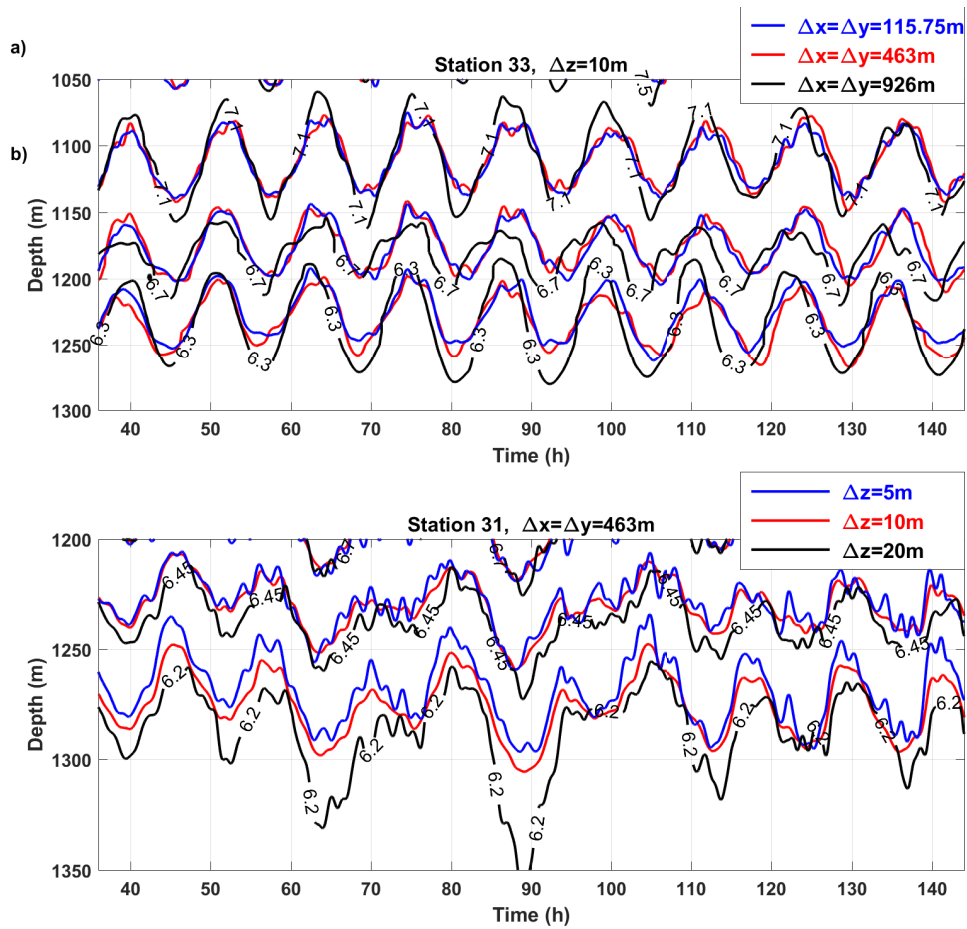


Figure 5: The model predicted time series at stations 33 a) and 31 b) for different horizontal a) and vertical b) grid steps. The model resolution is detailed in the figure legend.



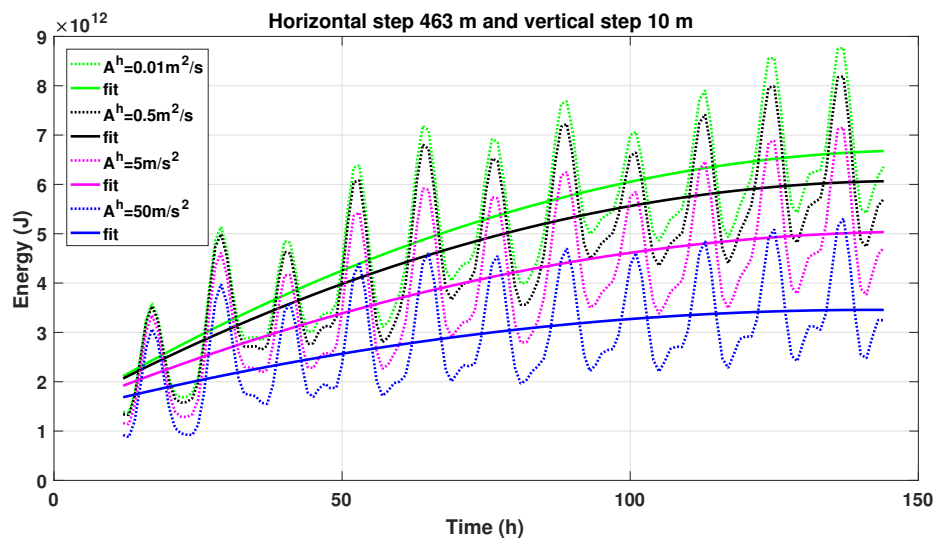


Figure 6: The domain integrated APE calculated for different values of horizontal viscosity coefficient.

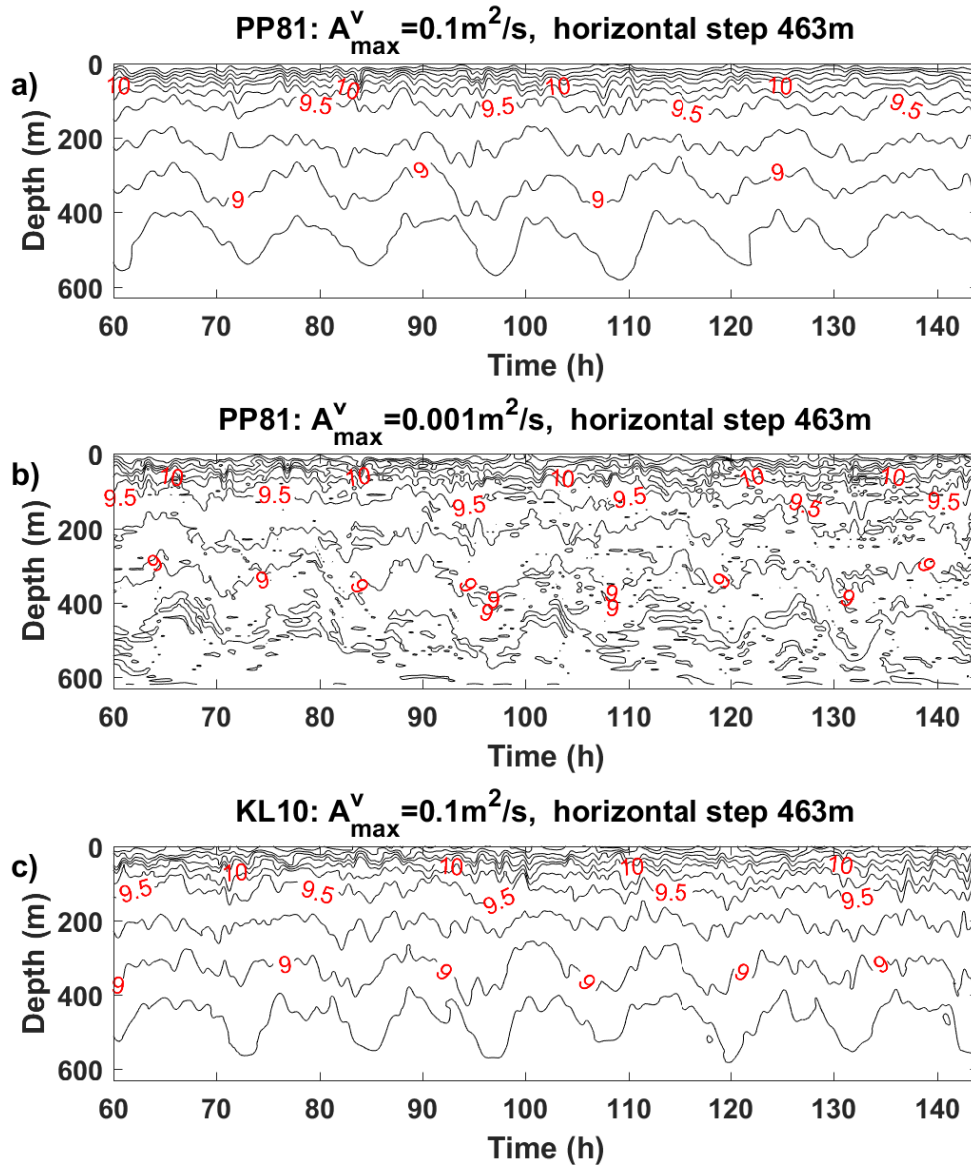


Figure 7: Sensitivity runs conducted with different vertical mixing parameterization schemes. The model predicted temperature time series were calculated for the point of CTD station 32 (Figure 1).

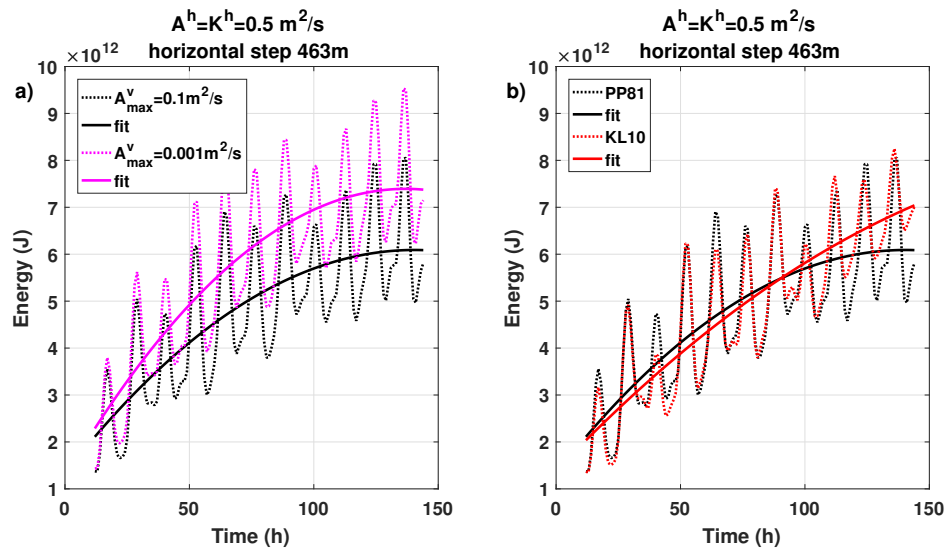


Figure 8: The domain integrated APE time series for different viscosity coefficients and parameterization schemes (Pacanowski and Philander (1981) and Klymak et al. (2013)) calculated at the position of CTD station 32.