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Highlights

Energetics of tidally induced internal waves over isolated seamount

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- The study focuses on the tidal energy conversion to internal waves over an isolated seamount.
- Sensitivity runs were conducted in a wide range of the numerical grid resolution.
- The coarse grid models overestimate available potential energy converted to internal waves.

Energetics of tidally induced internal waves over isolated seamount

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Abstract

Tidally generated internal waves over Rosemary Bank Seamount, North Atlantic, were investigated using the Massachusetts Institute of Technology general circulation model. The model results were validated against in-situ data collected during the 136th cruise of the RRS 'James Cook' in June 2016. The current study focuses on the sensitivity of the model output to the parameter settings. The estimates of the available potential energy integrated over the model domain were taken as a proxy for evaluating the sensitivity of the model results to the grid steps, horizontal and vertical viscosity, diffusivity, and mixing schemes. It was found that coarse grid models overestimate available potential energy converted to internal tides over seamounts. In fact, the energy conversion rate from barotropic to baroclinic tidal components is sensitive to the grid resolution. The reasons for this tendency are discussed in the paper.

Keywords:

Internal tide, Rosemary Bank Seamount, Numerical modelling

1 1. Introduction

The principal sources of the tidal energy conversion from barotropic to baroclinic motions are located over oceanic ridges, continental slopes and seamounts. These areas provide a basic income to the baroclinic wave energy, which ultimately converts into internal water mixing and provides the conditions for setting the global oceanic circulation (Munk and Wunsh, 1998). Analysis of the parameterization of internal wave effects for setting the global oceanic stratification was recently estimated by MacKinnon et al.

(2017). The authors discussed tidally induced mixing over bottom obsta-9 cles and estimated how much tidal energy is radiated to the far-field with 10 internal waves. The lee wave mechanism of internal wave generation was the 11 focus of this study. This scenario takes place under supercritical tidal con-12 ditions when the tidal flow is strong enough to arrest the generated internal 13 waves in the area of topographic features. The modelling results presented 14 by MacKinnon et al. (2017) assume that further steps in the parameteriza-15 tion of water mixing are required for making the model predictions accurate. 16 A very detailed analysis of the tidal energy conversion and contribution of 17 higher baroclinic modes to the energy balance was conducted recently by Vic 18 et al. (2019). Using a semi-analytical model, the authors found that higher 19 baroclinic tidal modes can account for up to 27% of tidal energy conversion. 20 Note that coarse-grid ocean models cannot resolve internal lee waves and 21 short-scale internal modes. As a consequence, these processes are missing in 22 model energy estimates. However, the comparison of fine and coarse resolu-23 tion model outputs can evaluate the effect of the sub-grid baroclinic process 24 on the energy budget. The model settings can be the same except for the 25 grid resolution in both cases. Such experiments help understand the role of 26 small-scale processes in water mixing and energy budget. 27

The present paper focuses on Rosemary Bank Seamount (RBS) located 28 in the North Atlantic, Figure 1. This case study aims to understand the 29 sensitivity of model predictions to the model settings. 136th cruise of the 30 RV "James Cook" was conducted in the RBS area in Mav-June 2016 (here-31 after JC136). The data collected during this cruise are considered in the 32 present paper. Specifically, we refer to the temperature, salinity, temperature 33 and velocity profiles recorded at three CTD-LADCP stations (Connectivity-34 Temperature-Depth, Lowered-Acoustic-Doppler-Current-Profiler). The po-35 sitions of oceanographic stations are shown in Figure 1a. 36

Theoretical analysis of the tidally induced internal waves around RBS 37 was reported in (Stashchuk and Vlasenko, 2021). It was found there that 38 internal wave dynamics, specifically, the wave generation and their propa-39 gation over RBS, can be treated in terms of two waveguides located in the 40 seasonal and main pycnoclines, Figure 1a. Specifically, the tidal flow in-41 teracting with a cluster of volcanic origin tall bottom cones located at the 42 RBS summit (see Figure 1 a) generates short-scale internal waves in subsur-43 face 100 m thick seasonal pychocline layer. Below 800m depth, i.e. in the 44 main pycnocline, Figure 1b, oscillating tidal flow generates bottom trapped 45 sub-inertial internal waves propagated counterclockwise around RBS. 46

The numerical experiments reported in (Stashchuk and Vlasenko, 2021) revealed a good agreement between the model and observational data. The present study is based on the concept of two waveguides reported in the paper mentioned above. The intensification of the baroclinic tidal signal in the surface and bottom layers is evident both in observations (Figure 2 a,b) and the model outputs (Figure 2 c,d).

The present study focuses on the requirements that should be applied 53 to large-scale modelling. In many global ocean models, the horizontal grid 54 resolution is relatively coarse, several kilometres in the best-case scenario. 55 The model requirements for simulations of tidally induced baroclinic motions 56 are more demanding. In many cases, the horizontal grid resolution should be 57 100 m or less for accurate replication of generated internal waves. The global 58 oceanic models are incapable of simulating internal tides with such grids on 59 global and regional scales (Robertson, 2006). We consider the RBS area as 60 a case study in the context of broader applications of the modelling efforts. 61 Structure wise, the paper is arranged as follows. It starts with the model 62 description. This section is followed by a discussion of the baroclinic tidal 63 energy estimation method. The grid resolution and the turbulent mixing 64 parameterizations are discussed in the section "Model results". Finally, the 65

⁶⁶ principal outcomes of the study are formulated in the concluding section.

67 2. The model

The modelling experiments were conducted using the fully non-linear non-68 hydrostatic Massachusetts Institute of Technology general circulation model 69 (MITgcm) (Marshall et al., 1997). The model domain, Figure 1 a, included a 70 815×698 numerical grid with horizontal resolution $115 \,\mathrm{m}$ in its central part. 71 A telescopic increase of the spatial resolution was arranged by adding extra 72 128 grid points to the lateral boundaries of the calculation area. In doing 73 so, a smooth increase of the horizontal resolution from 115 m in the central 74 part to $2 \cdot 10^8$ m at the periphery allowed to avoid the wave reflection from 75 the model boundaries. The water depth was restricted by 2000 m isobath in 76 the vertical direction. The vertical grid step was ten metres in all numerical 77 experiments. 78

The shaved cell method for the topography interpolation was used in the present study. Its advantage, compared to the traditional full step representation, is in the reduction of numerical errors induced by the incorrect bathymetry interpolation. This problem was discussed by Adcroft et al. (1997). It was demonstrated there that the shaved cell method for the topography interpolation shows a substantial improvement in the consistency of the model results with the observational data compared with the traditional full step topography representation. The partial cell capability can be used with the variable parameter called in the MITgcm as hFacMin (value between 0 and 1). It corresponds to the minimum fractional size of the cell. In the present calculation, we have been using hFacMin=0.2.

The tide forcing was activated in the model by a tidal potential added 90 to the right-hand side of the momentum balance equations. The details of 91 the method are described in (Vlasenko and Stashchuk, 2021). Considering 92 that M₂ tidal signal predominates in the RBS area, we restricted our analysis 93 using only principal semidiurnal tidal forcing. The tidal input parameters 94 were set using the data taken from the inverse tidal model TPXO 8.0 (Egbert 95 and Erofeeva, 2002). The model was run with a steady, uniform horizontal 96 stratification assuming no initial horizontal pressure gradients. 97

The Richardson number dependent parametrization, PP81, was used for the coefficients of vertical viscosity A^h and diffusivity K^h (Pacanowski and Philander, 1981). The details are as follows:

$$\begin{array}{rcl}
A^{v} &=& \frac{A^{v}_{0}}{(1+a\mathrm{Ri})^{n}} + A^{v}_{b}, \\
K^{v} &=& \frac{A^{v}}{(1+a\mathrm{Ri})} + K^{v}_{b}.
\end{array} \tag{1}$$

Here Ri is the Richardson number, $Ri = N^2(z)/(u_z^2 + v_z^2)$, and u and v are 101 the components of zonal and meridional horizontal velocities, respectively. 102 The background mixing/viscosity model parameters A_b and K_b were set at 103 the minimum level to provide the conditions for internal waves generation 104 and propagation: $A_b^v = 10^{-5} \text{ m}^2 \text{ s}^{-1}$ and $K_b^v = 10^{-5} \text{ m}^2 \text{ s}^{-1}$. The adjustable parameters were: $A_0^v = 1.5 \cdot 10^{-2} \text{ m}^2 \text{ s}^{-1}$, a=5 and n=1. This set of model 105 106 parameters revealed the excellent performance of the MITgcm in replication 107 of tidally generated internal waves (Stashchuk et al., 2014; Stashchuk and 108 Vlasenko, 2017; Vlasenko et al., 2014, 2018). 109

The PP81 parameterization increases the coefficients A^v and K^v in the areas with small Richardson numbers, which dumps shear instabilities and smooths inverse water stratification produced by breaking internal waves. It also allows setting the upper limit of the vertical viscosity coefficient A_{max}^v . In this study A_{max}^v was taken at the level of $0.1 \text{ m}^2 \text{s}^{-1}$.

The vast majority of the model runs in this study were conducted for the time interval of six days (144 hours) with the constant horizontal viscosity A^{h} and diffusivity K^{h} coefficients equals $0.5 \text{ m}^{2} \text{ s}^{-1}$. Additional sensitivity runs were done in a wide range of diffusivity/viscosity parameters. They are discussed below.

Computing wise, one-hour outputs were arranged for all three-dimensional fields. In addition, vertical profiles of temperature and horizontal velocities were recorded with one-minute sampling at some selected points. Their positions coincide with the CTD-LADCP stations.

124 3. Tidal energy estimation method

The tidal energy conversion rate from barotropic to baroclinic component depends on many factors. They are the intensity of the tidal flow, water stratification, the shape of bottom topography, background mixing processes, etc. The sink of tidal energy to internal waves and ultimately to water mixing can be quantified in terms of internal tidal energy generated over the bottom topography.

In many cases, it is not easy to separate the barotropic tidal signal from the baroclinic one. Specifically, this is true when velocities are recorded over an inclined three-dimensional bottom topography. In this case, the separation procedure can introduce a significant error.

The residual currents generated by tides can lead to extra uncertainty in 135 the calculations of a vertical mean tidal velocity. Specifically, this concerns 136 the case of bottom trapped waves. Such a case was reported by Lerczak et 137 al. (2003) who studied internal wave dynamics at the Mission Beach (USA). 138 Analysing the ADCP data, they found differences in the structure of along-139 shore and cross-shore tidal currents. The authors pointed out that separating 140 the barotropic tidal signal from the baroclinic one should be used with cau-141 tion, particularly in regions with significant topographic variations. Note 142 that the estimates of available potential energy produced by tides are less 143 sensitive to the barotropic component. The analysis presented below is based 144 on the estimation of the APE. 145

Several methods are used for the APE calculations. A comprehensive analysis of the procedures applied to internal wave fields was presented by Kang and Fringer (2010). Three commonly used methods for the APE estimates suggested by Lorenz (1955), Gill (1982), and Holliday and McIntyre (1981) are considered in this paper. It was found that the method reported by Holliday and McIntyre (1981) is the most accurate in the calculation of the APE for internal waves. Their technique is based on the Taylor series ¹⁵³ analysis. The recommended formula for the APE estimates is as follows:

APE =
$$\frac{g^2 \rho'^2}{2\rho_0 N^2} + \frac{g^3 (N^2)_z \rho'^3}{6\rho_0^2 N^6} + O(\rho'^4).$$
 (2)

Here ρ' is the perturbation of density to its equilibrium state.

Algorithm (2) was used in this paper. The APE calculations were conducted every one hour using the model outputs. The graphs are presented below in the following sections. Technically, the APE was calculated by vertical and horizontal integration over the whole model domain. The quadratic polynomial fit that includes the three nearest grid points best fits for the volume integrated APE and presents the long-term trend

¹⁶¹ 4. Model results

The sensitivity of the model output to the horizontal and vertical grid 162 resolution is reported in this section. The principal point of this study is: 163 what the horizontal and vertical grid steps Δx and Δz should be taken to 164 resolve the baroclinic tidal processes correctly? Vitousek and Fringer (2011) 165 have shown that the ability of the model to reproduce small-scale nonhydro-166 static physical processes depends on the leptic ratio coefficient, $\lambda \equiv \Delta x/h_1$. 167 Here h_1 is the depth of the interface/pycnocline. For an accurate replication 168 of the internal wave dynamics produced by non-hydrostatic models, the value 169 of the leptic ratio λ should be at the level of O(1) (Vitousek and Fringer. 170 2011). 171

Considering these requirements, one should mention that the water stratification in the RBS area has two principal elements shown in Figure 1 b: a shallow 100-metre depth seasonal pycnocline and the main pycnocline located below 1000 m depth. The latter is weaker but occupies a much larger part of the water column.

Numerically wise, both values of h_1 for seasonal and main pychoclines can 177 be taken to estimate the leptic ratio. These estimates can help in the choice 178 of the model resolution. The principal question is: what processes should 179 be replicated by the model? The fine resolution modelling allows consider-180 ing a wide variety of small-scale dynamics, both short-scale internal waves 181 developed in seasonal pycnocline and bottom trapped internal tidal waves. 182 These requirements are not always possible for global-scale models. We con-183 sider a range of grid settings to illustrate models' abilities to replicate the 184 wide-scale baroclinic tidal motions. The study discusses fine-scale resolution 185

model experiments and analyses the coarser grid runs used in global oceanmodels.

188 4.1. Sensitivity to the grid resolution

An example of the model sensitivity to the grid resolution is shown in 189 Figure 3. The model temperature time-series at station 32 (Figure 1a) was 190 calculated with different horizontal grid steps, 111.75 m, 463 m, and 926 m. 191 They are presented in panels a, b, and c of Figure 3, respectively. This figure 192 reveals that the ability of the model to capture short internal waves in the 193 upper seasonal pycnocline layer decreases with the increase of horizontal grid 194 steps. However, the numerical scheme still works well with coarser resolution 195 and reproduces long wave oscillations. Note that long-term wave amplitudes 196 increase with the increase of the horizontal grid steps. 197

How sensitive are the tidally induced baroclinic motions and water mixing 198 to the model resolution? The coarser grid model predictions of internal tidal 199 energy could differ from that estimated in the fine-resolution experiments. 200 The influence of the horizontal step on the value of APE is illustrated in 201 Figure 4a. Here a six-day time series of the depth-integrated model domain 202 APE calculated for the horizontal resolution $\Delta x = \Delta y = 111.75 \text{ m}, 463 \text{ m}, \text{ and}$ 203 926 m are presented. The parameters $A^h = K^h$ in these experiments were 204 $0.5 \,\mathrm{m^2 \, s^{-1}}$, and the vertical resolution Δz was equal to 10 m. 205

The common feature of all three graphs is the evidence of tidal periodicity. The fit curves to these periodical oscillations show the steady growth of the APE. However, after six days of tidal motion, the system ultimately arrives at a stationary state.

The coarser grids usually dump short internal waves, which reduces the APE in the numerical predictions. At the same time, coarser grids do not affect the generation of long internal waves, which are more energetic than short-scale waves. To have some quantitative estimates, a series of numerical experiments with different grid resolutions, horizontal and vertical, was conducted to study the sensitivity of the model outputs to the model grid parameters.

The APE time series for a wide range of model resolution with horizontal grid steps from 115 m to 926 m, and vertical grid steps from 5 m to 20 m are presented in Figures 4 a and 4 b. These figures show the spin-up of the model over about 150 hours. The model comes to a stationary regime at the end of this time interval, although the domain integrated APE is sensitive to the model resolution. It is generally higher at coarser grids.

There are several explanations for this result. The first one can be found 223 considering the domain volume. The latter is sensitive to the grid resolution. 224 It varies with changing vertical and horizontal model grid steps, Figure 4 c 225 and 4d. The MITgcm is a Z-coordinate model which approximates the 226 bottom as a step-wise function. The bottom topography in Z-coordinate 227 models and the total water volume varies depending on the grid resolution. 228 For instance, the total volume of water in the model domain for the coarser 229 experiment shown in Figure 4 exceeds the fine-resolution volume for more 230 than 2%. In addition, the topography in the coarser grid is steeper. The 231 increase of the bottom steepness results in the generation of more energetic 232 bottom-trapped internal waves, Figure 3. 233

The confirmation of the APE growth due to roughening of topography is seen in Figure 4 b. It shows the domain-integrated APE time series for three different vertical grid steps, 5 m, 10 m, and 20 m. Quantitatively, decreasing the vertical resolution in Z-coordinate models increases the water volume in the regions of sloping topography. As a result, the total APE calculated at coarser grids is higher, Figure 4 d. Making the vertical resolution thinner leads to improvements in the replication of the bottom flow dynamics.

Considering some local characteristics (not the domain integrated), the 241 sensitivity of the model output to the grid resolution can be more detailed. 242 Two examples of this sensitivity are shown in Figure 5. The model predicted 243 temperature calculated at the positions of CTD stations 31 and 33 shows the 244 consistency of all time-series considered with different horizontal and verti-245 cal grid resolutions. The tidal nature of vertical oscillations is clearly seen in 246 these records. All curves reveal in-phase tidal periodicity. The amplitudes of 247 vertical oscillations for all model outputs are also comparable. That could 248 be evidence that coarse grid models can capture the main energy contributor 249 with acceptable accuracy. At the same time, decreasing horizontal and verti-250 cal model resolution introduces some more details that can be very important 251 for predicting local marine environment parameters. 252

²⁵³ 4.2. Sensitivity to horizontal mixing parameterization

The time series of the model predicted APE calculated for different model settings, e.g. diffusivity, viscosity and grid resolution, are compared in this section. By making the grid finer, at some stage the model output starts to be insensitive to further reduction of the grid step.

Figures 6 shows the domain integrated APE and its best fit for different values of the viscosity coefficients: $0, 0.01, 0.5, 50 \text{ m}^2 \text{s}^{-1}$. All curves presented

here show that the tidal energy increases gradually after the model starts. 260 The spin-up period, 150 hours, is shown in Figure 6. The system becomes 261 stationary when the pumping tidal energy is balanced by dissipation. As 262 we found, the model predicted volume integrated APE capacity in the area 263 does depend on the horizontal mixing parameterization. For the horizontal 264 mixing/viscosity coefficients between $0.01 \text{ m}^2 \text{s}^{-1}$ and $50 \text{ m}^2 \text{s}^{-1}$ the APE level 265 varies in the range of 100 %, Figure 6. This fact should be taken into account 266 in the interpretation of large-scale circulation modelling results. 267

268 4.3. Experiments with vertical mixing schemes

In large-scale models, the energy cascading along the spectrum is generally provided, introducing parameterization schemes for vertical viscosity and diffusivity. One of them is the Richardson number based parameterization (1) included in the MITgcm package as a standard option. It shows a good performance for internal tide modelling in many studies, e.g. Vlasenko et al. (2014, 2016, 2018); Vlasenko and Stashchuk (2018).

Field measurements (Polzin et al., 1997) have revealed that vertical mix-275 ing does not occur uniformly over the oceans. It is normally enhanced near 276 rough topographies due to the generation of internal waves that convert 277 to turbulence. The lower level background mixing develops at the level of 278 $\sim 10^{-5} \text{m}^2 \text{s}^{-1}$ over the whole ocean interior (Ledwell et al., 1998; Gregg, 1989). 279 This value can be three orders of magnitude larger **over rough topography** 280 features, (Polzin et al., 1997). To have a comparison, the results presented 281 below show the model outputs calculated for two MITgcm build-in vertical 282 mixing schemes. In all experiments, the horizontal grid resolution was 463 m. 283

284 4.3.1. Richardson number dependent scheme PP81

The Richardson number dependent parameterization for vertical mixing (1) was used in this study. The value 0.1 m² s⁻¹ of the maximum permissible viscosity coefficient A_{max}^v was taken in this study. This requirement is applied in the MITgcm setting for the areas with strong vertical mixing, assuming possible density inversions. Note that the background turbulent mixing was set at the level of $A_b^v = 10^{-5}$ m² s⁻¹ and $K_b^v = 10^{-5}$ m² s⁻¹ in the whole area.

The sensitivity of the model outputs to the viscosity coefficient A_{max}^v was checked by changing this parameter within a two-order range. The result is shown in Figure 7. It illustrates that the increase of A_{max}^v from 0.001 to 0.1 m² s⁻¹ leads to stabilizing of the model output. Comparing the time series of temperature records calculated for Station 32 with different A_{max}^v coefficients, Figures 7 a and 7 b, indicates that the choice $A_{\text{max}}^v=0.1 \text{ m}^2 \text{ s}^{-1}$ shows a more stable model output.

299 4.3.2. KL10 mixing scheme

Klymak and Legg (2010) developed an original mixing scheme that is 300 focused on the effect of breaking internal waves and does not include the 301 Richardson-number criterion. This scheme assumes that energy dissipa-302 tion is governed by the equivalence of the density overturning scales to the 303 Ozmidov scale. Eddy diffusivity and viscosity are estimated using the Os-304 born relation (Osborn, 1980). This method yields a simple parameterization 305 $Kz = 0.2L_T^2 N$, where L_T is the size of vertical density overturns. This 306 method is included in the MITgcm as the KL10 package. It was scrutinized 307 by Klymak et al. (2013) that this parameterization does not account for 308 shear-driving mixing. 309

A series of experiments were conducted in the present study with KL10 mixing scheme. An example of typical time series of the APE calculated for station 32 is shown in Figure 7 c. For the comparison, panels a and b show similar time series calculated using the PP81 scheme with different maximum permissible viscosity coefficients A^v . All other model parameters were the same in these experiments.

Note that at a local scale, a two-order decrease of the maximum vertical 316 viscosity coefficient results in the appearance of instabilities that are visible in 317 the time series, Figure 7b. Comparison of Figures 7a and 7b indicates that 318 the choice $A_{\max}^v = 0.1 \text{ m}^2 \text{ s}^{-1}$ is the more realistic one producing a more stable 319 vertical structure (without inversions) usually observed in the ocean. The 320 KL10 parameterization reproduces both long-period internal waves in the 321 bottom layer and short-period waves in the surface layer quite successfully, 322 Figure 7 b, although the signal looks less regular than that produced by the 323 PP81 scheme, Figure 7 a. 324

Figure 8 b shows the APE time series obtained with the PP81 and KL10 schemes. Both APE curves are close to each other over 93 hours of the model run. However, after eight tidal cycles, the APE calculated using the KL10 scheme continues to grow above the already saturated APE level achieved by the PP81-scheme.

330 5. Discussion and conclusions

Tidal energy conversion from barotropic to baroclinic components is one of the principal driving forces of the global ocean mixing and meridional overturning circulation (Munk and Wunsh, 1998). This process is still not well resolved in global ocean models. Specifically, the question is to what extent the tidal energy conversion is sensitive to the models' settings. Grid resolution, vertical turbulent mixing parameterization, and horizontal viscosity/diffusion settings are critical for a robust model prediction.

In previous studies, the authors achieved a good agreement between the 338 model outputs and field observations (Stashchuk et al., 2014; Stashchuk and 339 Vlasenko, 2017; Vlasenko et al., 2014, 2018). In this paper, a similar range of 340 input model parameters is used. In the RBS area, the comparative analysis 341 of model results and in situ data collected during JC136 cruise was reported 342 in (Stashchuk and Vlasenko, 2021). The consistency of the model outputs 343 with the in-situ collected data was demonstrated. The present paper con-344 siders the problem in a broader context, assuming that large-scale numerical 345 models usually use coarse numerical grids and can not include fine-scale baro-346 clinic processes. The present paper estimates the possible effect of numerical 347 grid resolution and turbulent mixing parameterization schemes on the model 348 output. The principal aim was to find the range of the model applicability 349 and its sensitivity to the input parameter settings. 350

It was found that the increase of the grid step leads to a damping of 351 the generation of short internal waves. This result was entirely expected, 352 assuming higher numerical viscosity at coarser grids. A surprising outcome 353 was the increase of the domain integrated APE at coarser numerical grids. 354 The answer was found in terms of the model topography variations presented 355 at different grid resolutions. Z-coordinate numerical models reproduce the 356 bottom topography steeper at coarser grids, affecting the model performance 357 and intensifying the generated waves. 358

The estimates of the tidally induced kinetic energy (K) accumulated in 359 the area over one tidal cycle has shown the following results: $K = 3.814 \cdot 10^{13}$ J 360 for the grid $\Delta x = \Delta y = 115.75 \,\mathrm{m}, K = 3.8337 \cdot 10^{13} \mathrm{J}$ for the grid $\Delta x =$ 361 $\Delta y = 463 \text{ m}$, and $K = 4.0357 \cdot 10^{13} \text{ J}$ for the grid $\Delta x = \Delta y = 926 \text{ m}$. The 362 vertical resolution dz and the background horizontal viscosity A_{b}^{v} were the 363 same in all these experiments, i.e. $dz = 10 \,\mathrm{m}$ and $A_b^v = 0.5 m^2 s^{-1}$, respec-364 tively. Thus, it was found that both available potential energy and the kinetic 365 energy increase in the model outputs on coarser grids. 366

The energy conversion rate from barotropic tidal component to internal waves in the RBS area was estimated. The calculations were conducted using the methodology suggested by Kelly et al. (2010); Zhang et al. (2017). The energy conversion EC for the domain $L_x \times L_y$ was calculated as:

$$EC = \int_0^{L_x} \int_0^{L_y} \left\langle p' \vec{U} \nabla H \right\rangle \, dx dy. \tag{3}$$

Here $\langle . \rangle$ means the time-averaging over one tidal cycle, \vec{U} is the depth-371 averaged horizontal velocity, and p' is the wave-induced pressure perturba-372 tion. It was found that $EC = 3.35 \cdot 10^8$ W for a grid $\Delta x = \Delta y = 115.75$ m. 373 $EC = 3.32 \cdot 10^8$ W for the grid resolution $\Delta x = \Delta y = 463$ m, and $EC = 2.97 \cdot 10^8$ W 374 for the grid $\Delta x = \Delta y = 926 \,\mathrm{m}$. The vertical step for all considered experi-375 ments was the same, equals $\Delta z = 10$ m. Our experiments clearly show that 376 the energy conversion rate from surface tides to baroclinic motions is under-377 estimated in coarser grid experiments. 378

A similar analysis of the sensitivity of the energy conversion rate to the 379 horizontal grid spacing was conducted by Niwa and Hibiya (2011) (for Global 380 Ocean) and Zilberman et al. (2009) (for the Mid-Atlantic Ridge). These au-381 thors used quite a different numerical approach than applied in the present 382 paper. Specifically, the terrain-following sigma-coordinate hydrostatic mod-383 els were applied to these calculations. It was found there that the tidal energy 384 conversion rate integrated over the global ocean (Niwa and Hibiya, 2011) and 385 local area in the Brazil Basin (Zilberman et al., 2009) increases with the re-386 duction of the model grid spacing. This conclusion is in line with the results 387 reported here obtained by using the z-coordinate MITgcm model. 388

A methodological outcome from this study is that simple estimations of 389 the available potential energy and the total kinetic energy generated by the 390 tides over RBS show the increase of these values on coarser model grids, 391 Figure 6 a and b. At the same time, the estimates of the energy conversion 392 rate from barotropic to internal tide reveal that the coarser grids reduce the 393 efficiency of the tidal energy conversion. There is no contradiction between 394 these two tendencies. Analysis of Figure 4c and 4d shows that the coarser 395 grids incorporate larger volumes of water with the increase of the grid step. 396 In fact, with the coarser grids, the topography's tidal activity is different 397 from that simulated over the fine-resolution topography. 398

A series of numerical experiments were also conducted to test the model output's sensitivity to the choice of diffusivity/viscosity model coefficients.

Water mixing parameterization is critical for accurately modelling various 401 processes, from microscopic to global atmospheric and oceanic scales. In the 402 present study, we used the Richardson-number dependent parameterization 403 scheme PP81. This turbulent closure scheme provides the APE saturation 404 over eight tidal cycles. The Osborn relation based scheme KL10 also re-405 vealed a similar performance over 7.5 tidal periods. Note that its further 406 performance over ten tidal cycles did not demonstrate any tendency to reach 407 the stationary level. In general, the usage of two vertical turbulent mixing 408 schemes, PP81 and KL10, did not significantly differ the model output over 400 several tidal cycles, although the KL10 closure model shows a higher internal 410 tidal energy saturation level. 411

412 6. Acknowledgement

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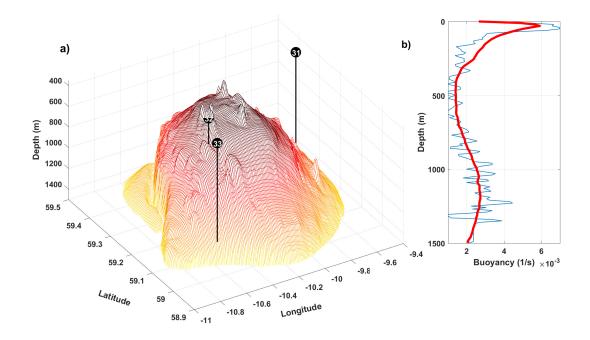


Figure 1: a) Bottom topography of Rosemary Bank Seamount (RBS) with the location of CTD stations 31, 32, and 33 conducted during the 136th cruise of the RV "James Cook". b) The buoyancy frequency recorded in the RBS area is shown in blue. The smoothed buoyancy frequency profile used in the modelling is shown in red.

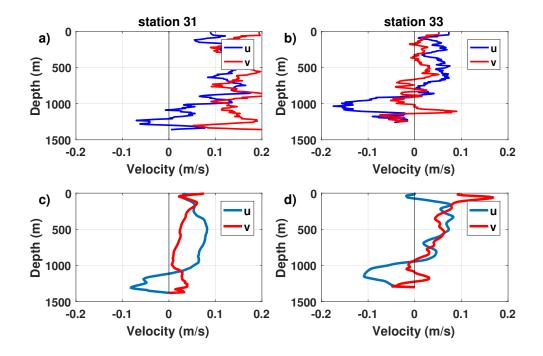


Figure 2: Vertical profiles of zonal (blue) and meridional (red) velocities recorded by the LADCP at 31-st and 33-rd CTD stations (panels a and b, respectively). Panes c and d present the same profiles but replicated by the numerical model.

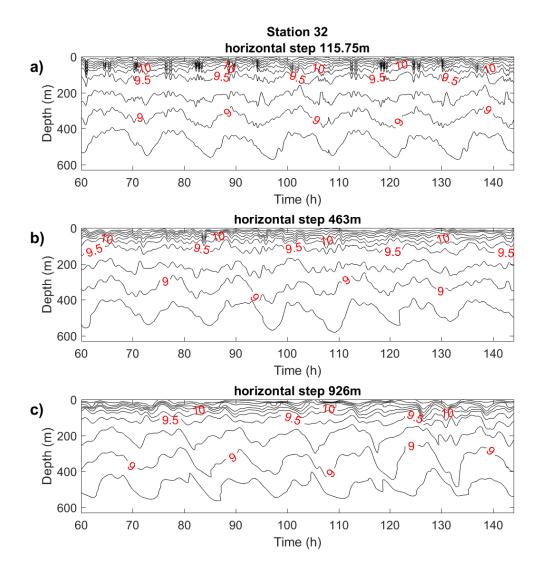


Figure 3: Temperature time series reproduced by the MITgcm at the 32-nd CTD station (the position is shown in Figure 1). The horizontal grid step in these experiments was 115.75 m, 463 m, and 926 m (panels a, b, c, respectively).

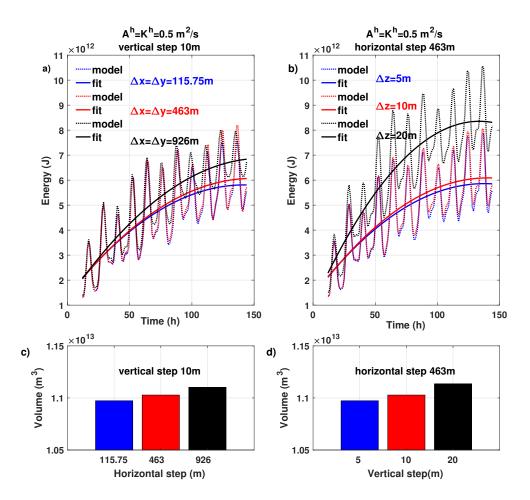


Figure 4: a) Model predicted available potential energy (APE) calculated for the RBS area with a different vertical grid resolution: 115.75m (blue), 463m (red) and 926m (black). b) The same, but calculated with different vertical steps: 5m (blue), 10m (red) and 20m (black). c) and d) The volume of the model domain calculated for different horizontal and vertical grid resolutions. The values are shown in the graph.

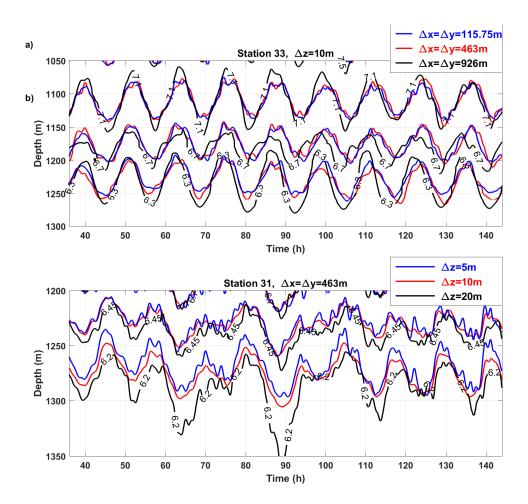


Figure 5: The model predicted time series at stations 33 a) and 31 b) for different horizontal a) and vertical b) grid steps. The model resolution is detailed in the figure legend.

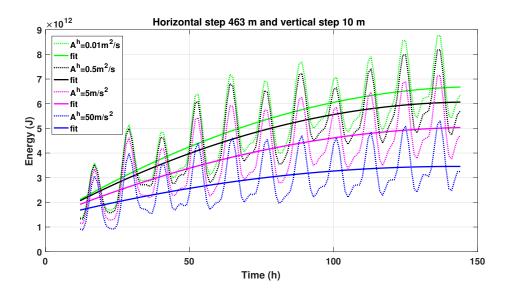


Figure 6: The domain integrated APE calculated for different values of horizontal viscosity coefficient.

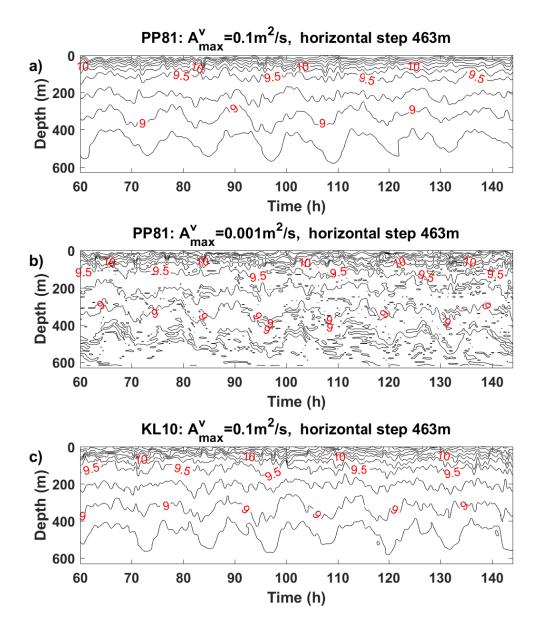


Figure 7: Sensitivity runs conducted with different vertical mixing parameterization schemes. The model predicted temperature time series were calculated for the point of CTD station 32 (Figure 1).

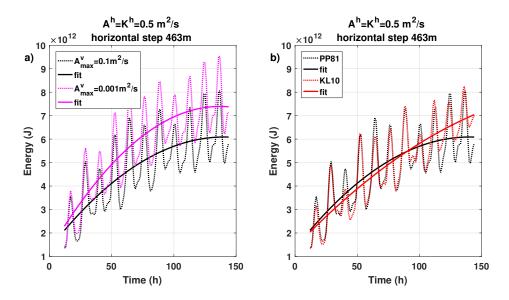


Figure 8: The domain integrated APE time series for different viscosity coefficients and parameterization schemes (Pacanowski and Philander (1981) and Klymak et al. (2013)) calculated at the position of CTD station 32.