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# Ethanol Steam Reforming for Hydrogen Production Over Hierarchical Macroporous Mesoporous SBA-15 Supported Nickel Nanoparticles

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## Abstract

The influence of complementary macropores, present in hierarchical macroporous mesoporous SBA-15, on the performance of supported Ni nanoparticles for ethanol steam reforming has been investigated. The increased open nature of the architecture, afforded through the incorporation of the secondary macropore network, enables superior metal dispersion. This, in turn, enhances catalytic hydrogen production performance through the generation of a greater density of active sites.

**Keywords** Hierarchical porous materials · Macroporous mesoporous SBA-15 · Hydrogen production · Ethanol steam reforming · Nickel · Nanoparticles

## 1 Introduction

Hydrogen represents a clean and potentially sustainable fuel, which can address increasing uncertainties regarding the availability and accessibility of fossil fuel reserves.

Furthermore, a hydrogen-based energy economy could address concerns regarding the impact of fossil fuel combustion on climate change, which itself is driving such research into alternative fuel feedstocks [1]. As such, the development of alternative environmental friendly renewable fuels is vital to meeting legally mandated targets for EU CO<sub>2</sub> emissions [2]. Biomass has been widely accepted as a sustainable chemical feedstock, with hydrogen derived from catalytic bioethanol steam reforming acknowledged to be a viable production route [3]. The development of novel catalytic systems, with optimal on-stream performance and stability, is, therefore, a key parameter to enabling this future process for sustainable fuel production.

Low-cost-earth-abundant base metals, such as Ni, are commonly the active site of choice for ethanol steam reforming (ESR) due to superior economics [4], but routinely suffer on-stream deactivation by coking and sintering [5, 6]. Fine-tuning of reaction conditions can inhibit carbon deposition, through increased process temperature or addition of O<sub>2</sub> to drive coke oxidation, but at the expense of increased potential for active site sintering, operating costs, or active site oxidation [7]. Alternatively, modifying the chemical nature of the support structure provides a second strategy to address coke accumulation. Alkali metal or alkali earth metal promoters switch-off ethanol dehydration and ethylene polymerisation, through tuning of the acid/base nature [7], in contrast acidic supports, such as zeolites, enhance ethanol dehydration the formation of ethylene increase coking and deactivation [6]. Basic oxides of Ca and Mg have been

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used to increase  $H_2$  production performance via sorption-enhance steam reforming [8, 9], praseodymium and barium oxides have also promoted enhance steam reforming activity through reduced Ni sintering [10, 11], whereas rare earth and transition metal oxides, e.g.  $CeO_2$  or  $ZrO_2$ , impart labile surface oxygen which assists oxidation of carbon deposits to  $CO_2$  [12]. The ratio of these to the active phase playing an important role in Ni crystallite size, which in turn controls activity and resistance to carbon deposition [13]. Such reducible oxide materials typically exhibit low intrinsic surface areas, and as such are ineffective for stabilising highly dispersed base metal active sites, whilst porous analogues typically suffer reduced hydrothermal stability. Alternative approaches have been to co-deposit these oxides in conjunction with the active Ni species [14–16], yet these could result in a capping layer on top of the active species, whereas adlayer oxide growth has also shown potential to address the inherent issues of these oxides [17].

We have previously demonstrated the capacity of silica as a support material in ESR, with its intrinsic high surface area and chemically inertness, for both commercial and simple sol–gel synthesised silica, enabling high active site dispersion [18], and accessibility [19]. These beneficial attributes can be further enhanced through the utilisation of ordered mesoporous silicas, such as SBA-15, SBA-16 and KIT-6, which have demonstrated superior active site generation whilst overcoming internal mass diffusion constraints for C4 and C9 alcohols [20]. Controlling ESR performance over Ni deposited on SBA-15 is dependent on the location of the active species. Sintering and coking are apparent where the active site exists as large nanoparticles located on the external surfaces of the support skeleton, with nanoparticle size > mesopore diameter [15]. Whilst promoters (including Ce, Au, Ca, or Mg [14, 21, 22]) afford one strategy to tackle this undesirable phenomenon, encapsulating the Ni active species provides an alternative, for example, successfully incorporating the Ni sites within the mesopores of SBA-15 or KIT-6 [23]. Control of the location of the Ni species in this way prohibits sintering, via confinement, with the more open 3-dimensional architecture of KIT-6 also mitigating against pore blockage through coking, resulting in high on-stream stability. The incorporation of ethylene glycol within the impregnation protocol being critical, similarly, EDTA has recently been shown to assist in crystallite size control [24].

The incorporation of a complementary macropore network within SBA-15, to yield macroporous mesoporous SBA-15 (MM-SBA-15), has shown to be beneficial for both active site dispersion and internal mass diffusion of bulk substrates for liquid-phase catalytic selective oxidation reactions [25]. Here we further demonstrate the benefit of this

secondary structural framework within MM-SBA-15 for the gas-phase catalytic ESR over deposited Ni nanoparticles.

## 2 Experimental

MM-SBA-15, comprising a framework of 400 nm spherical macropores with a two-dimensional hexagonal close-packed assembly of mesopore channels ( $P6mm$ ), was synthesised by the method of Dhainaut et al. [26] MM-SBA-15 was doped with Ni nanoparticles, via a glycol assisted impregnation to enhance metal dispersion, and screened for catalytic hydrogen production from ESR [23].

### 2.1 400 nm Polystyrene Nanosphere Synthesis

Styrene ( $50\text{ cm}^3$ ) and divinylbenzene ( $9.5\text{ cm}^3$ ) were each washed three times with sodium hydroxide solution (0.1 M, 1:1 vol/vol) followed by three washings with deionised water (1:1 vol/vol) to remove the polymerisation inhibitors. The washed organic phases were added to degassed deionised water ( $377\text{ cm}^3$ ), purged under  $N_2$  ( $10\text{ cm}^3\text{ min}^{-1}$ ), at  $70\text{ }^\circ\text{C}$ . An aqueous initiator solution of potassium persulfate (0.16 g) in deionised water ( $12\text{ cm}^3$ ) was added dropwise, and the resulting mixture stirred at 300 rpm under  $N_2$  ( $10\text{ cm}^3\text{ min}^{-1}$ ) for 18 h. The solid polystyrene nanospheres were isolated by filtration and washed with deionised water.

### 2.2 MM-SBA-15 Synthesis

Pluronic P123 (10 g) was dissolved in deionised water ( $75\text{ cm}^3$ ) and hydrochloric acid (2 M,  $290\text{ cm}^3$ ) with stirring at  $35\text{ }^\circ\text{C}$ . Polystyrene beads (45 g) were added to the solution and left to stir for 1 h. Tetraethoxysilane ( $22.8\text{ cm}^3$ ) was added and left for 20 h with agitation at 500 rpm. The resulting sol–gel was aged within a sealed container for 24 h at  $80\text{ }^\circ\text{C}$  under static conditions. The solid was filtered, washed with deionised water ( $1000\text{ cm}^3$ ) and dried at room temp before calcination at  $550\text{ }^\circ\text{C}$  for 6 h in air (ramp rate  $0.5\text{ }^\circ\text{C min}^{-1}$ ).

### 2.3 Ethylene Glycol Assisted Ni Impregnation

MM-SBA-15 (1.5 g) was stirred in aqueous impregnation solution (12 ml) containing nickel nitrate hexahydrate to give metal loadings of 10, 5 and 2.5 and 1 wt% and ethylene glycol (1:1 Ni:glycol mol ratio) for 16 h. The solution was heated to  $50\text{ }^\circ\text{C}$  and stirred for 8 h to form a dry powder. The resulting solid was calcined at  $400\text{ }^\circ\text{C}$  for 2 h in air (ramp rate  $1\text{ }^\circ\text{C min}^{-1}$ ) followed by reduction at  $600\text{ }^\circ\text{C}$  for 2 h under flowing hydrogen (ramp rate  $1\text{ }^\circ\text{C min}^{-1}$  hydrogen flow  $10\text{ cm}^3\text{ min}^{-1}$ ).

## 2.4 Characterisation

Powder X-ray diffraction (XRD) patterns were collected on a Bruker D8 Advance Diffractometer with a LynxEye high-speed strip detector using Cu K $\alpha$  (1.54 Å) radiation, Si(111) monochromated, Ni filter and calibrated to quartz. Low-angle data were collected between  $2\theta = 0.45^\circ$ – $8^\circ$  and wide-angle data between  $2\theta = 10^\circ$ – $80^\circ$ . Nitrogen adsorption–desorption isotherms were recorded on a Quantachrome Autosorb IQTPX porosimeter with analysis using ASiQwin v3.01 software. Samples were degassed at  $150^\circ\text{C}$  for 12 h prior to recording N<sub>2</sub> adsorption/desorption isotherms. BET surface areas were calculated over the relative pressure range 0.02–0.2 with microporosity assessed by the t-plot method over the range  $P/P_0 = 0.2$ – $0.5$ . Mesopore properties were calculated by the fitting of isotherms to the relevant DFT kernel within the software package. XPS analysis was performed using a Kratos Axis SUPRA XPS fitted with a monochromated Al K $\alpha$  X-ray source (1486.7 eV). Survey scans were recorded at a pass energy of 160 eV, and high-resolution scans recorded at a pass energy of 20 eV. Electronic charge neutralization was achieved using a magnetic immersion lens. All sample data was recorded at a pressure below  $10^{-8}$  Torr and a room temperature of 294 K. Data was analysed using CasaXPS v2.3.19PR1.0. High resolution scanning transmission microscopy (STEM) images were obtained on an aberration-corrected JEOL 2100-F microscope operated at 200 kV, with image analysis using ImageJ 1.41 software. Samples were dispersed in methanol and drop cast on 200-mesh carbon coated copper grids and dried under ambient conditions.

## 2.5 Catalytic Screening

Ethanol steam reforming for hydrogen production was carried out using a two-stage fixed-bed reaction system. The two stages were heated externally using two heaters (each one has a diameter of 25 mm and length of 150 mm) and controlled individually. During the experiment,  $100\text{ ml min}^{-1}$  N<sub>2</sub> gas (controlled by a mass flow meter) was used as the carrier gas. 0.2 g catalyst was placed into the second reactor and heated by the second furnace to  $600^\circ\text{C}$ , while the first furnace (quartz wool was placed inside for enhancing the dispersion of vapours) was heated to  $200^\circ\text{C}$ . The gas hourly space velocity was  $6000\text{ h}^{-1}$ .

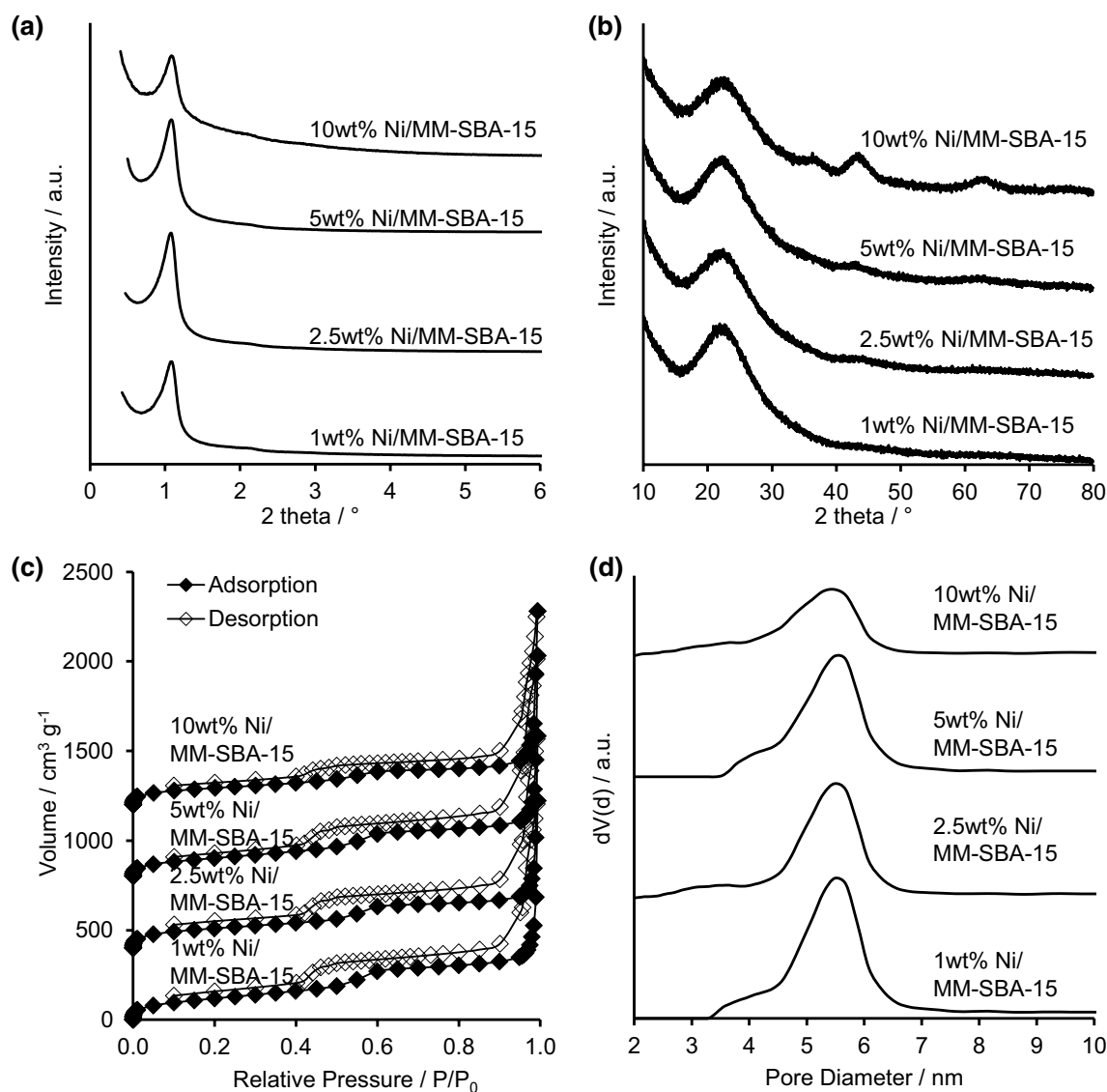
When temperatures stabilized, a mixture of ethanol and water (molar ratio 1:4, total flow rate of  $3\text{ ml h}^{-1}$ ) was injected using a syringe pump into the first reactor to be vaporised. The vapours passed through the second reactor for catalytic reforming reactions. The products produced from the second reactor were cooled using a condensation system (air and dry ice cooled) to collect the liquid products. The non-condensable products (H<sub>2</sub>, CO and CO<sub>2</sub>) were

analysed on-lined by an ETG Syngas Analyser MCA 100. Experiments were repeated in triplicate to confirm catalytic performance reproducibility. Initial and steady-state hydrogen productivity was calculated from the average hydrogen production over 0–0.16 and 0.5–1.5 h respectively.

To confirm that we were not operating under reagent limiting conditions, full or equilibrium limited conversion [27], simulations to evaluate reaction equilibrium were determined using Aspen Plus®. An Idea model was used, for which a Gibbs reactor was employed at  $600^\circ\text{C}$  and 1 atmosphere with a mixture of ethanol and water (molar ratio of 1:4) at a flow rate of  $3\text{ g h}^{-1}$ , with possible products consistent with the literature [28].

## 3 Results and Discussion

The physicochemical properties of the Ni-MM-SBA-15 catalysts series were evaluated by XRD and nitrogen adsorption–desorption isotherms, shown in Fig. 1. The d10 reflection in the low-angle XRD pattern (Fig. 1a) indicates a *P6mm* ordered mesopore structure, with a constant cell parameter of  $\sim 9.3\text{ nm}$  irrespective of Ni loading, which agrees with our previous studies [25, 26]. Wide-angle XRD (Fig. 1b) revealed the presence of both Ni and NiO phases, with Ni[111] reflection at  $43.9^\circ$  and NiO[111] at  $36.9^\circ$ , witnessed for loadings great than 2.5 wt%. Unfortunately, the presence of both phases prevents Scherrer average particle size evaluation due to the overlap of the NiO[200] and Ni[111] reflections. The presence of NiO is attributed to the storage conditions, since the catalysts were stored in air after reduction, and was also apparent for similarly prepared Ni/SBA-15 series [23]. Furthermore, this oxidation indicates that the ethylene glycol was fully removed during the synthesis's thermal processing steps [29]. Nitrogen adsorption isotherms, in Fig. 1c, reveal all catalytic materials exhibit type 4 isotherms with H1 hysteresis, which is typical of mesoporous materials comprising uniform diameter channel pores. Brunauer–Emmett–Teller (BET) surface areas showed an inverse correlation with metal loading, spanning from  $420\text{ m}^2\text{ g}^{-1}$  to  $330\text{ m}^2\text{ g}^{-1}$  for 1 and 10 wt% Ni loading respectively. These represent a maximum loss of 31% relative to the unfunctionalized parent, which has a surface area of  $478\text{ m}^2\text{ g}^{-1}$ , whereas intermediate loadings exhibit surface areas of  $392$  (2.5 wt%) and  $363$  (5 wt%)  $\text{m}^2\text{ g}^{-1}$  respectively. T-plot analysis, to deconvolute the contribution of microporosity to the total surface area, confirmed that the BET surface areas are contributed to solely from mesoporosity and macroporosity, with the complementary microporosity present in conventional cooperative self-assemble synthesized mesoporous SBA-15 absent [30, 31]. Average mesopore diameters of 5.6 nm across the series are consistent with



**Fig. 1** Characterisation of Ni/MM-SBA-15 catalysts series; **a** stacked low angle powder XRD offset for clarity, **b** stacked wide angle powder XRD offset for clarity, **c** stacked nitrogen adsorption–desorption

isotherms offset by 400 (2.5 wt%), 800 (5 wt%) and 1200 (10 wt%)  $\text{cm}^3 \text{g}^{-1}$ , and **d** stacked mesopore size distribution plot offset for clarity

the literature and exhibit monomodal pore size distributions, shown in Fig. 1d.

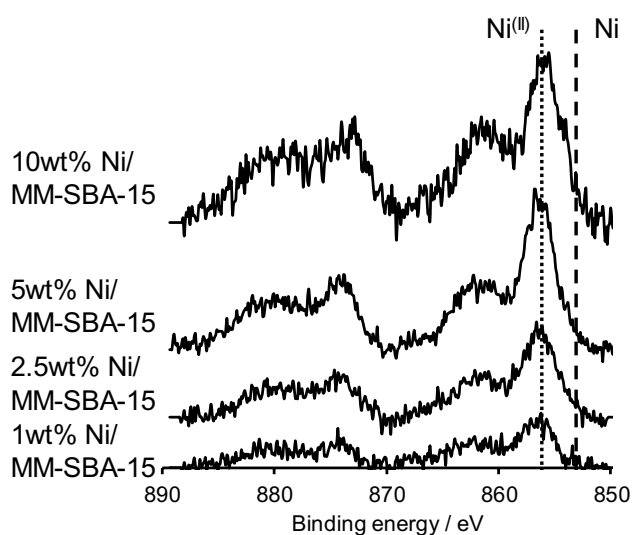
XPS was utilised to further investigate the chemical nature of the Ni active sites, shown in Fig. 2. As observed previously for purely mesoporous silica supports, the Ni species are predominately present as  $\text{Ni}^{\text{II}}$ , apparent from binding energy peak positions which are consistent with Ni  $2p_{3/2}$  NiO at 856 eV. Although all samples are subjected to a reduction step during Ni impregnation, storage in air at room temperature leads to significant nanoparticle oxidation.

Bright field STEM confirmed the presence of both macropores and mesopores within the support framework (Fig. 3), with the macropores acting to break up the mesopore domains, thus, decreasing the mesopore

channel length relative to conventional SBA-15 [32]. Average macropore diameters of 360 nm represent only a minor contraction, during calcination, of the hard template size of 390 nm, shown in Fig. 3b. This slight decrease is consistent with our previous investigations, with a decrease typically around 10% [33]. Figure 2c, d clearly reveal the hexagonal close packed arrangement of cylindrical channels of the mesostructures, as expected for SBA-15 [34], confirming the  $P6mm$  space group assigned by low angle XRD.

The open pore architecture afforded by MM-SBA-15 results in exceptional Ni dispersions, with Ni nanoparticles deposited throughout the material. High angle annular dark field STEM (Fig. 4), reveals the Ni nanoparticles as the brightest features due to the Z-contrasting nature of the



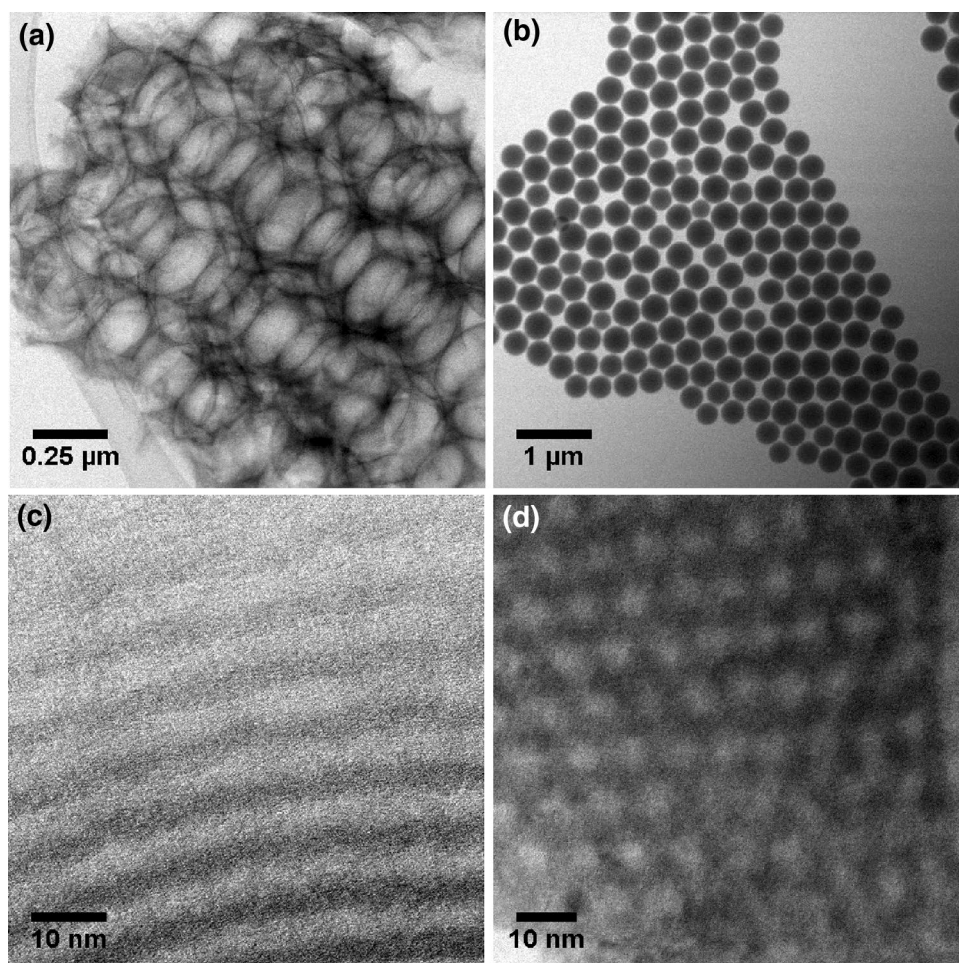


**Fig. 2** Stacked Ni 2p XPS spectra offset for clarity, with binding energies of Ni metal and NiO indicated

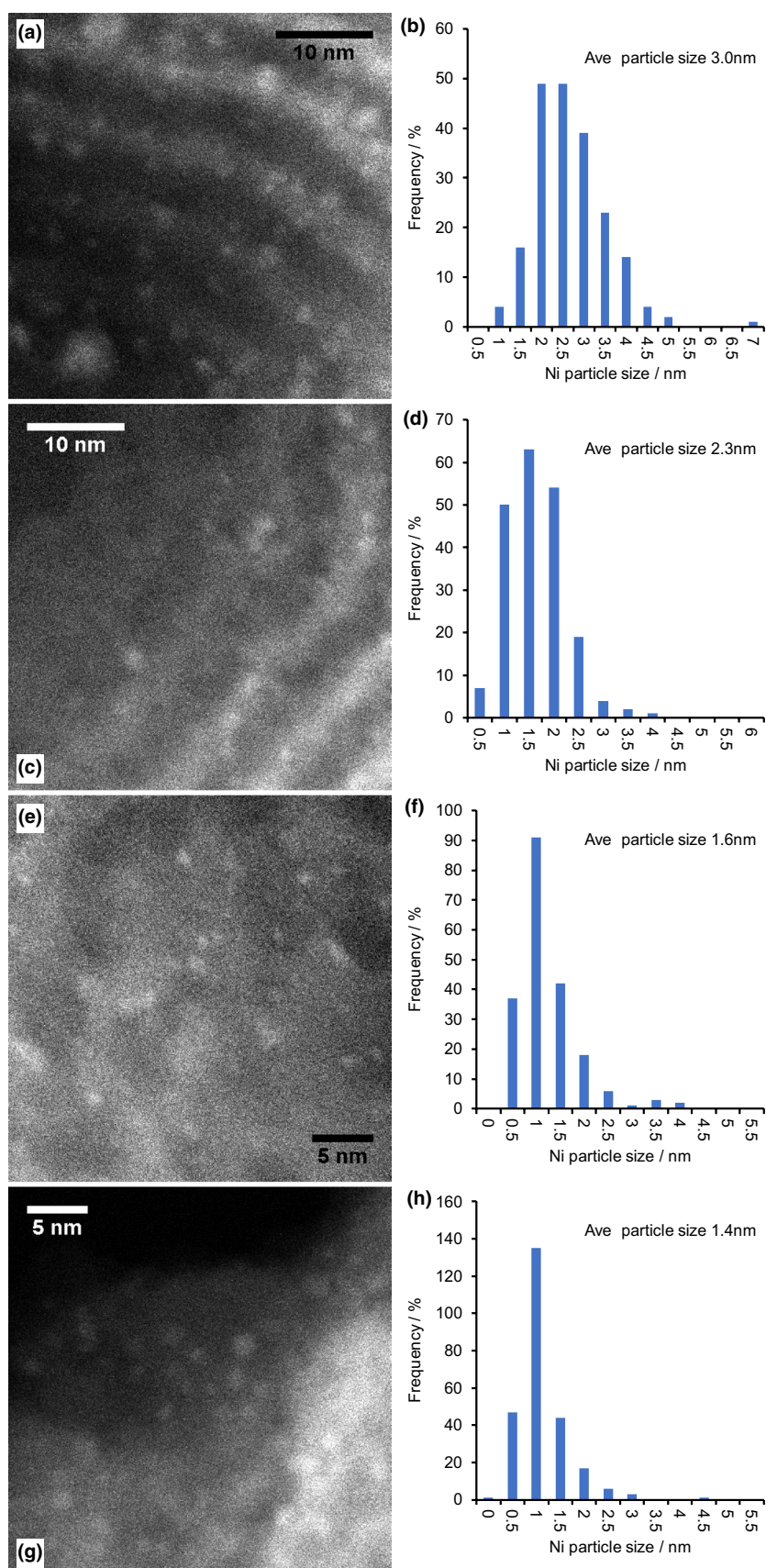
technique [35]. Average Ni particle sizes range from 1.4 to 3.0 nm for 1 and 10 wt% loading respectively, with all sample showing reasonably monomodal size distributions (Fig. 4b, d, f, and h). These sizes are considerably smaller than the average mesopore diameters, consistent with our study employing the ethyl glycol assisted impregnation for mesoporous only supports [23], and differ to non-assisted impregnated Ni/SBA-15 [15, 36]. Comparing our hierarchical MM-SBA-15 to the conventional SBA-15, we see a significant enhancement in Ni dispersion for the macroporous mesoporous framework. This decrease in average Ni nanoparticle size opens up more sites for catalysis, representing a more efficient utilisation of the support's available surface area.

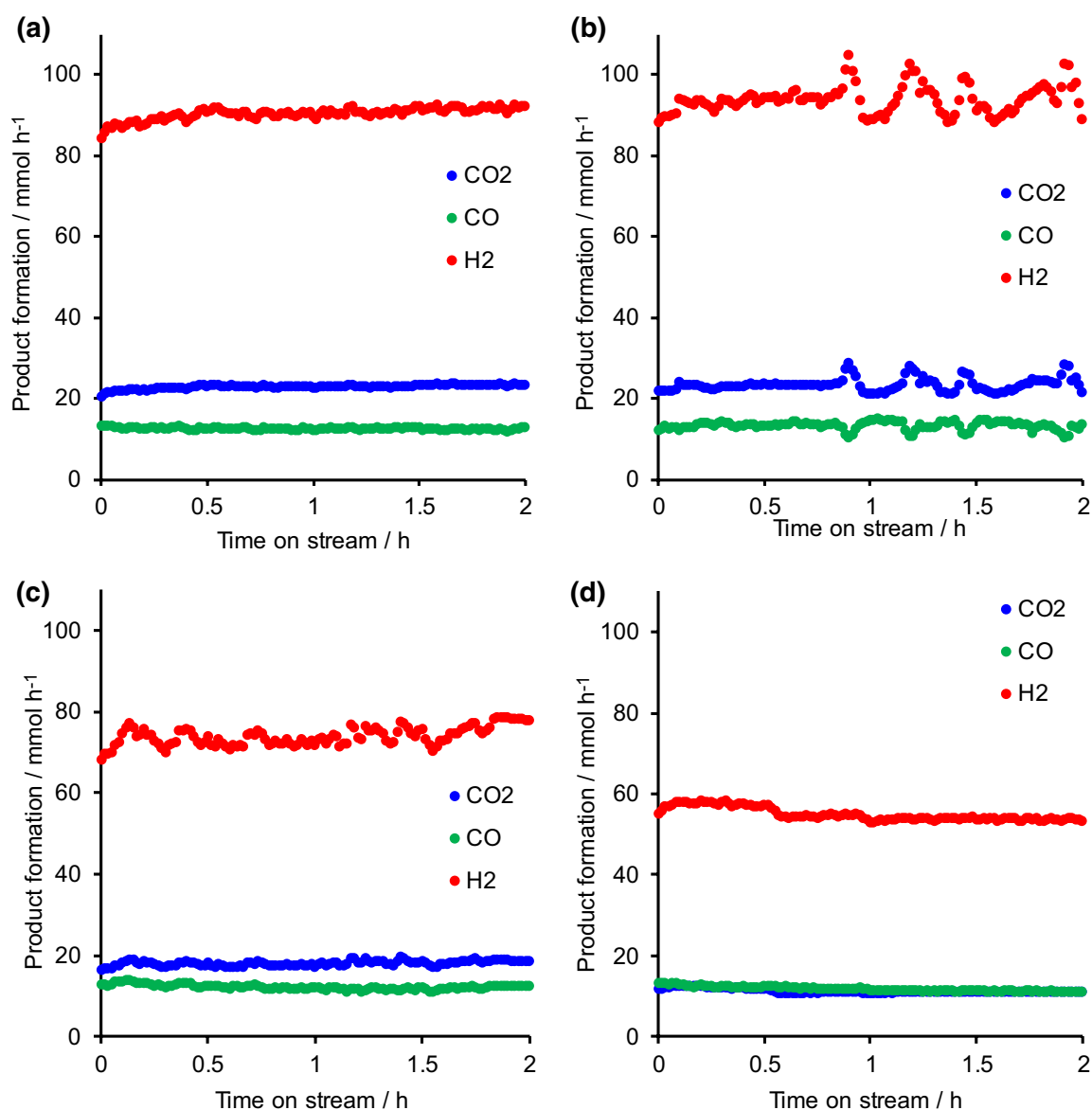
The performance of our Ni/MM-SBA-15 catalyst series for hydrogen production, from ESR, was evaluated as a potential route for sustainable production [37].  $H_2$  production was evaluated at 600 °C, identical conditions to those used in our previous studies, to quantify initial activity and on-stream deactivation over the initial 2 h of the reaction (Fig. 5).

**Fig. 3** Bright field STEM of MM-SBA-15; **a** macropore structure, **b** polystyrene macropore hard template, **c** mesopore channels, and **d** hexagonal packing of mesopores



**Fig. 4** HAADF-STEM and Ni particle size distribution of **a**, **b** 10 wt% Ni/MM-SBA-15, **c**, **d** 5 wt% Ni/MM-SBA-15, **e**, **f** 2.5 wt% Ni/MM-SBA-15, **g**, **h** 1 wt% Ni/MM-SBA-15



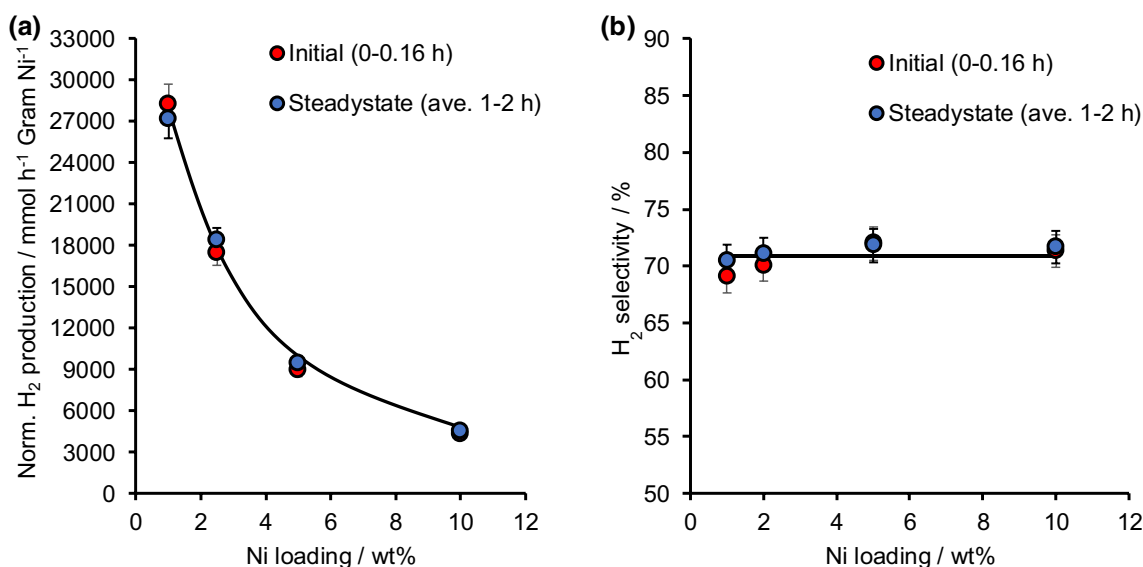


**Fig. 5** Hydrogen production from ESR over **a** 10 wt% Ni/MM-SBA-15, **b** 5 wt% Ni/MM-SBA-15, **c** 2.5 wt% Ni/MM-SBA-15, and **d** 1 wt% Ni/MM-SBA-15

This relatively short on-stream time frame represents the period over which considerable losses in performance were previously observed for conventional SBA-15, with up to a 50% decrease observed. The time on-stream profiles show unvarying hydrogen production across all four catalysts, with overall hydrogen production increasing with metal loading. This absence in observed deactivation reflects the highly beneficial role of macropore incorporation for this gas-phase reaction. The capacity of macroporosity to overcome coking (the deactivation route occurring in conventional SBA-15) is particularly striking given the relative dimensions of substrate and products (0.38 nm) and mesopore (5.5 nm) respectively. Furthermore, we can rule out a difference in

on-stream stability to be a size effect, direct comparison of equal Ni particles sizes (10 wt% Ni/MM-SBA-15 vs 2.5 wt% Ni/SBA-15) show deactivations of ~0% vs 50% respectively. This also discredits differences in other physicochemical properties of the Ni sites being responsible, as these can be assumed to be comparable given the identical synthesis protocols and equal mesopore structure. Given that ~90% of the surface area in MM-SBA-15 is within the mesopores [38], the vast majority of the Ni can be expected to reside within these. Therefore, we conclude that the beneficial role of the macropores in preventing deactivation is diffusion driven, with the shortened mesopore domains resulting in a decrease in residence time of the substrate/products and





**Fig. 6** **a** mass normalised initial and steady-state productivity of Ni/MM-SBA-15 and **b** initial and steady-state hydrogen selectivity of Ni/MM-SBA-15

thus a decrease in potential for coke formation [39]. It is also worth noting that under our reaction conditions, ethanol conversion is not equilibrium limited, confirmed by simulation and in agreement with the literature [40, 41]. Therefore, an optimal ethanol conversion of 65% (5 wt% Ni/MM-SBA-15) validates that our reaction conditions are reagent limited [27].

Mass normalised H<sub>2</sub> productivity averaged over the initial 10 min of the reaction revealed an inverse correlation with loading (Fig. 6a). This MM-SBA-15 series shows enhancement in performance of up to 80%, and an average across the series of 60% (for comparable loading), when benchmarked against our previously reported conventional SBA-15 [23]. The performance of these materials is also considerably greater than citric acid assisted sol-gel Ni/SiO<sub>2</sub> and Ni/SBA-15 prepared via aqueous incipient wetness impregnation (1375 and 850 mmol h<sup>-1</sup> g<sub>Ni</sub><sup>-1</sup> respectively) [15, 19]. The superior activity arises from a smaller Ni particle size, from higher metal dispersions, which is likely to result in the formation of unique ensembles which presumably favour a higher density of low coordination sites and is consistent with a size sensitive active species, as previously proposed. Quantitative comparison of these initial activities and steady-state activities confirms the absence of deactivation.

As observed previously for our Ni/SBA-15 and Ni/KIT-6 catalyst families, the Ni/MM-SBA-15 series displays a common hydrogen selectivity of 70% (Fig. 6b), with CO and CO<sub>2</sub> formation in approximately a 1:1 ratio. This common selectivity across this series (and our previous investigation [23]) is indicative of a common reforming mechanism that is

independent of nickel particle size, support, and also time on stream when deactivation is absent.

## 4 Conclusions

The incorporation of secondary macropore networks within mesoporous SBA-15, via a hard-templating strategy, yields an excellent catalyst support framework for ESR. Highly dispersed Ni nanoparticles within our MM-SBA-15 skeleton show excellent activity and selectivity for hydrogen production. The open architecture for the bimodal porous support material enables superior Ni dispersion during catalyst preparation, which subsequently imparts improved performance, both initially and under steady-state conditions, with the latter due to support resistance to on-stream deactivation.

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